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# ICC-ES Evaluation Report

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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

**DIVISION: 05 00 00—METALS** 

Section: 05 05 19—Post-Installed Concrete Anchors

**REPORT HOLDER:** 

**INVESTMENTS HARDWARE LIMITED (IHL)** 

# **EVALUATION SUBJECT:**

INVESTMENTS HARDWARE LIMITED (IHL)
OCTOPLATINUM ADHESIVE ANCHOR SYSTEM AND
POST-INSTALLED REINFORCING BAR SYSTEM IN
CRACKED AND UNCRACKED CONCRETE

# 1.0 EVALUATION SCOPE

# Compliance with the following codes:

- 2021, 2018, 2015, 2012 and 2009 International Building Code<sup>®</sup> (IBC)
- 2021, 2018, 2015, 2012 and 2009 International Residential Code<sup>®</sup> (IRC)

For evaluation for compliance with codes adopted by Los Angeles Department of Building and Safety (LADBS), see ESR-4931 LABC and LARC Supplement.

# Property evaluated:

Structural

# **2.0 USES**

The Investments Hardware Limited (IHL) OCTOPLATINUM Adhesive Anchor System is used as anchorage and the Post-Installed Reinforcing Bar System is used as reinforcing bar connection (for development length and splice length) in cracked and uncracked normalweight concrete with a specified compressive strength,  $f_c$ , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa) to resist static, wind or earthquake (IBC Seismic Design Categories A through F) tension and shear loads.

The anchor system complies with anchors as described in Section 1901.3 of the 2021, 2018 and 2015 IBC, Section 1909 of the 2012 IBC and is an alternative to cast-in-place and post-installed anchors described in Section 1908 of the

2012 IBC, and Sections 1911 and 1912 of the 2009 IBC. The anchor system may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the IRC.

The post-installed reinforcing bar system is an alternative to cast-in-place reinforcing bar connection governed by ACI 318 and IBC Chapter 19.

# 3.0 DESCRIPTION

### 3.1 General:

The IHL OCTOPLATINUM Adhesive Anchor System and Post-Installed Reinforcing Bar System is comprised of IHL OCTOPLATINUM two-component adhesive filled in cartridges, static mixing nozzles, dispensing tools, hole cleaning equipment and adhesive injection accessories, and steel anchor elements, which are continuously threaded steel rods (to form the IHL OCTOPLATINUM Adhesive Anchor System) or deformed steel reinforcing bars (to form the IHL OCTOPLATINUM Adhesive Anchor System or the Post-Installed Reinforcing Bar System).

The primary components of the IHL OCTOPLATINUM Adhesive Anchor System and Post-Installed Reinforcing Bar System, including the IHL OCTOPLATINUM adhesive cartridge, static mixing nozzle, and steel anchor elements, are shown in Figures 1 and 2 of this report. The manufacturer's printed installation instructions (MPII), included with each adhesive unit package, are shown in Figure 6 of this report.

# 3.2 Materials:

3.2.1 IHL **OCTOPLATINUM** Adhesive: OCTOPLATINUM adhesive is an injectable two-component vinylester-urethane hybrid adhesive. The two components are kept separate by means of a labelled dual-cylinder cartridge. The two components combine and react when dispensed through a static mixing nozzle, supplied by IHL, which is attached to the cartridge. IHL OCTOPLATINUM is available in coaxial cartridges of 9.5-ounce (280 mL), and side-by-side cartridges of 28-ounce (825 mL).

Each cartridge label is marked with the adhesive expiration date. The shelf life, as indicated by the expiration date, applies to an unopened cartridge stored in a dry, dark, and cool environment.



# 3.2.2 Hole Cleaning Equipment:

- **3.2.2.1 Standard Equipment:** Hole cleaning equipment is comprised of steel wire brushes supplied by IHL, and air blowers which are shown in Figure 6 of this report. The IHL dust extraction system shown in Figure 3 of this report removes dust with a HEPA dust extractor during the hole drilling and cleaning operation.
- **3.2.2.2 IHL Hollow Drill Bit System:** The IHL hollow drill bit system shown in Figure 3 is comprised of Heller Duster Expert Hollow drill bit with carbide tips conforming to ANSI B212.15 attached to a class M vacuum that has a minimum air flow rating of 90cfm (150m³/h resp. 42l/s). The vacuum dust extractor system removes the drilling dust during the drilling operation, eliminating the need for additional hole cleaning.
- **3.2.3 Dispensers:** IHL OCTOPLATINUM adhesive must be dispensed with manual dispensers, pneumatic dispensers, or electric powered dispensers supplied by IHL Anchoring GmbH.

### 3.2.4 Steel Anchor Elements:

- 3.2.4.1 Threaded Steel Rods for use in Post-Installed Anchor Applications: Threaded steel rods must be clean and continuously threaded (all-thread) in diameters described in Tables 4 and 10, and Figure 6 of this report. Specifications for grades of threaded rod, including the mechanical properties, and corresponding nuts and washers, are included in Table 2 of this report. Carbon steel threaded rods must be furnished with a minimum 0.0002-inch-thick (0.005 mm) zinc electroplated coating complying with ASTM B633, SC1 or a minimum 0.0021-inch-thick (0.053 mm) mechanically deposited zinc coating complying with ASTM B695, Class 55. The stainless steel threaded rods must comply with Table 2 of this report. Steel grades and types of material (carbon, stainless) for the washers and nuts must match the threaded rods. Threaded steel rods must be clean, straight and free of indentations or other defects along their length. The embedded end may be flat cut or cut on the bias to a chisel point.
- **3.2.4.2** Steel Reinforcing Bars for use in Post-Installed Anchor Applications: Steel reinforcing bars must be deformed reinforcing bars as described in Table 3 of this report. Tables 7 and 13 and Figure 6 summarize reinforcing bar size ranges. The embedded portions of reinforcing bars must be clean, straight, and free of mill scale, rust, mud, oil and other coatings (other than zinc) that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation except as set forth in ACI 318-19 Section 26.6.3.2 (b), ACI 318-14 Section 26.6.3.1 (b) or ACI 318-11 Section 7.3.2, as applicable, with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.
- **3.2.4.3** Steel Reinforcing Bars for Use in Post-Installed Reinforcing Bar Connections: Steel reinforcing bars used in post-installed reinforcing bar connections must be deformed reinforcing bars (rebars) as depicted in Figures 4 and 5. Tables 16, 17, and Figure 6 summarize reinforcing bar size ranges. The embedded portions of reinforcing bars must be clean, straight, and free of mill scale, rust, mud, oil and other coatings that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation, except as set forth in Section 26.6.3.2(b) of ACI 318-19, Section 26.6.3.1(b) of ACI 318-14 or Section 7.3.2 of ACI 318-11, as applicable, with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.
- **3.2.4.4 Ductility:** In accordance with ACI 318-19 Section 2.3, ACI 318-14 Section 2.3 or ACI 318-11 Appendix D Section D.1, as applicable, in order for a steel anchor

element to be considered ductile, the tested elongation must be at least 14 percent and reduction of area must be at least 30 percent. Steel elements with a tested elongation less than 14 percent or a reduction of area less than 30 percent, or both, are considered brittle. Specifications and physical properties of various steel materials are provided for threaded rods in Table 2 and for threaded rods in Table 3 of this report. Where values are nonconforming or unstated, the steel must be considered brittle.

# 3.3 Concrete:

Normalweight concrete must comply with Sections 1903 and 1905 of the IBC. The specified compressive strength of the concrete must be from 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

# 4.0 DESIGN AND INSTALLATION

# 4.1 Strength Design of Post-Installed Anchors:

**4.1.1 General:** The design strength of anchors under the 2021 IBC and 2021 IRC must comply with ACI 318-19 Section 17.5.1.2 and this report, except as required in ACI 318-19 Section 17.10. The design strength of anchors under the 2018 and 2015 IBC, as well as the 2018 and 2015 IRC, must be determined in accordance with ACI 318-14 and this report. The design strength of anchors under the 2012 and 2009 IBC, as well as the 2012 and 2009 IRC, must be determined in accordance with ACI 318-11 and this report.

Under the 2021 IBC and IRC, strength reduction factors,  $\phi$ , as given in ACI 318-19 Section 17.5.3, must be used for load combinations calculated in accordance with 2021 IBC Section 1605.1 and ACI 318-19 Section 5.3.

Under the 2018 and 2015 IBC and IRC, the strength design of anchors must comply with ACI 318-14 17.3.1 or 318-11 D.4.1, as applicable, except as required in ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable.

Design parameters are provided in Tables 4 through Table 15 of this report.

Under the 2018 and 2015 IBC and IRC, strength reduction factors,  $\phi$ , as given in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, must be used for load combinations calculated in accordance with Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable.

Under the 2012 and 2009 IBC and IRC, strength reduction factors,  $\phi$ , as given in ACI 318-11 D.4.4 must be used for load combinations calculated in accordance with ACI 318-11 Appendix C.

- **4.1.2 Static Steel Strength in Tension:** The nominal static steel strength of a single anchor in tension,  $N_{S\theta}$ , in accordance with ACI 318-19 17.6.1.2, ACI 318-14 17.4.1.2 or ACI 318-11 D.5.1.2, as applicable, and the associated strength reduction factors,  $\phi$ , in accordance with ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are provided in Tables 4, 7, 10 and 13 of this report for the corresponding anchor steel.
- **4.1.3 Static Concrete Breakout Strength in Tension:** The nominal static concrete breakout strength of a single anchor or group of anchors in tension,  $N_{cb}$  or  $N_{cbg}$ , must be calculated in accordance with ACI 318-19 17.6.2, ACI 318-14 17.4.2 or ACI 318-11 D.5.2, as applicable, with the following addition:

The basic concrete breakout strength of a single anchor in tension,  $N_b$ , must be calculated in accordance with ACI 318-19 17.6.2.2, ACI 318-14 17.4.2.2 or ACI 318-11 D.5.2.2, as applicable, using the values of  $k_{c,cr}$  and  $k_{c,uncr}$  as provided in Tables 5, 8, 11 and 14 of this report. Where analysis indicates no cracking in accordance with ACI 318-19

17.6.2.5, ACI 318-14 17.4.2.6 or ACI 318-11 D.5.2.6, as applicable,  $N_b$  must be calculated using  $k_{c,uncr}$  and  $\Psi_{c,N}$  = 1.0. For anchors in lightweight concrete see ACI 318-19 17.2.4, ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable. The value of  $f_c$  used for calculation must be limited to 8,000 psi (55 MPa) in accordance with ACI 318-19 17.3.1, ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable. The value of  $f_c$  used for calculation must be limited to 2,500 psi (17.2 MPa) maximum for metric reinforcing bars in cracked concrete. Additional information for the determination of nominal bond strength in tension is given in Section 4.1.4 of this report.

**4.1.4 Static Bond Strength in Tension:** The nominal static bond strength of a single adhesive anchor or group of adhesive anchors in tension,  $N_a$  or  $N_{ag}$ , must be calculated in accordance with ACI 318-19 17.6.5, ACI 318-14 17.4.5 or ACI 318-11 D.5.5, as applicable.

Bond strength values ( $\tau_{k,cr}$ ,  $\tau_{k,uncr}$ ) are a function of concrete compressive strength, concrete state (cracked, uncracked) and installation conditions (dry concrete, water-saturated concrete, water-filled holes). Special inspection level is qualified as periodic for all anchors except as shown in Section 4.3 of this report (the selection of continuous special inspection level does not provide an increase in anchor category or associated strength reduction factor for design). The following table summarizes the requirements:

CONCRETE	SIAIE	BOND	STRENGTH	CONCRETE COMPRESSIVE STRENGTH	PERMISSIBLE INSTALLATION CONDITIONS	ASSOCIATED STRENGTH REDUCTION FACTOR
					Dry concrete	фа
cracked		Tk,cr			Water-saturated concrete	φws
				f'c	Water-filled holes	фwf
70		Tk,uncr			Dry concrete	фа
uncracked					Water-saturated concrete	φws
5				Water- filled holes	фи	

Strength reduction factors for determination of the bond strength are given in Tables 6, 9, 12 and 15 of this report. Adjustments to the bond strength may also be made for increased concrete compressive strength as noted in the footnotes to the corresponding tables and this section.

The bond strength values in Tables 6, 9, 12 and 15 of this report correspond to concrete compressive strength  $f_c$  equal to 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi and 8,000 psi (17.2 MPa and 55 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c / 2,500)^{0.10}$  [For **SI**:  $(f_c / 17.2)^{0.10}$ ]. The value of  $f_c$  used for calculation must be limited to 2,500 psi (17.2 MPa) maximum for metric reinforcing bars in cracked concrete. Where applicable, the modified bond strength values must be used in lieu of  $\tau_{k,cr}$  and  $\tau_{k,uncr}$  in ACI 318-19 Equations (17.6.5.1.2b) and (17.6.5.2.1), ACI 318-14 Equations (17.4.5.1d) and (17.4.5.2) or ACI 318-11 Equations (D-21) and (D-22), as applicable.

The resulting nominal bond strength must be multiplied by the associated strength reduction factor  $\phi_d$ ,  $\phi_{WS}$  or  $\phi_{Wf}$ , as applicable.

- **4.1.5** Static Steel Strength in Shear: The nominal static steel strength of a single anchor in shear as governed by the steel,  $V_{\text{SB}}$ , in accordance with ACI 318-19 17.7.1.2, ACI 318-14 17.5.1.2 or ACI 318-11 D.6.1.2, as applicable, and the strength reduction factor,  $\phi$ , in accordance with ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are given in Tables 4, 7, 11 and 13 of this report for the corresponding anchor steel.
- **4.1.6 Static Concrete Breakout Strength in Shear:** The nominal static concrete breakout strength of a single anchor or group of anchors in shear,  $V_{cb}$  or  $V_{cbg}$ , must be calculated in accordance with ACI 318-19 17.7.2, ACI 318-14 17.5.2 or 318-11 D.6.2, as applicable, based on information given in Tables 5, 8, 12 and 14 in this report.

The basic concrete breakout strength of a single anchor in shear,  $V_b$ , must be calculated in accordance with ACI 318-19 17.7.2.2, ACI 318-14 17.5.2.2 or ACI 318-11 D.6.2.2, as applicable, using the values of d given in Tables 5, 8, 12 and 14 of this report for the corresponding anchor steel in lieu of  $d_a$ . In addition,  $h_{ef}$  must be substituted for  $\ell_e$ . In no case shall  $\ell_e$  exceed 8d. The value of  $f_c$  shall be limited to a maximum of 8,000 psi (55 MPa) in accordance with ACI 318-19 17.3.1, ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable.

- **4.1.7 Static Concrete Pryout Strength in Shear:** The nominal static pryout strength of a single anchor or group of anchors in shear,  $V_{cp}$  or  $V_{cpg}$ , shall be calculated in accordance with AC\_ 318-19 17.7.3, ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable.
- **4.1.8 Interaction of Tensile and Shear Forces:** For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318-19 17.8, ACI 318-14 17.6 or ACI 318-11 D.7, as applicable.
- **4.1.9 Minimum Member Thickness**  $h_{min}$ , **Anchor Spacing**  $s_{min}$ , **Edge Distance**  $c_{min}$ : In lieu of ACI 318-19 17.9.2, ACI 318-14 17.7.1 and 17.7.3 or ACI 318-11 D.8.1 and D.8.3, as applicable, values of  $s_{min}$  and  $c_{min}$  described in this report must be observed for anchor design and installation. The minimum member thicknesses,  $h_{min}$ , described in this report must be observed for anchor design and installation. For adhesive anchors that will remain untorqued, AC\_ 318-19 17.9.3, ACI 318-14 17.7.4 or ACI 318-11 D.8.4 applies, as applicable.

For anchors that will be torqued during installation, the maximum torque,  $T_{max}$ , must be reduced for edge distances

INSTALLATION 1	ORQUE SUBJECT	TO EDGE DIS	TANCE
NOMINAL ANCHOR SIZE, d	MINIMUM EDGE DISTANCE, c <sub>min</sub>	MINIMUM ANCHOR SPACING, Smin	MAXIMUM TORQUE, T <sub>max</sub>
<sup>5</sup> / <sub>8</sub> in. to 1 in.			
#5 to #8	1.75 in.		
M16 to M24	(44.5 mm)		
ø14 to ø25		5 <i>d</i>	0.45· <i>T</i> <sub>max</sub>
1 <sup>1</sup> / <sub>4</sub> in.		04	O. TO Tillax
#9 to #10	2.75 in.		
M27 to M30	(70 mm)		
ø28 to ø32			

less than the values given in Tables 5, 8, 11 and 14 as applicable.  $T_{max}$  is subject to the edge distance,  $c_{min}$ , and anchor spacing,  $s_{min}$ , and shall comply with the following requirements:

For values of  $T_{max}$ , see Figure 6 of this report.

4.1.10 Critical Edge Distance  $c_{ac}$  and  $\psi_{cp,Na}$ : The modification factor  $\psi_{cp,Na}$ , must be determined in accordance with ACI 318-19 17.6.5.5, ACI 318-14 17.4.5.5 or ACI 318-11 D.5.5.5, as applicable, except as noted below:

For all cases where  $c_{Na}/c_{ac}$ <1.0,  $\psi_{cp,Na}$  determined from ACI 318-19 Eq. 17-6.5.5.1b, ACI 318-14 Eq. 17.4.5.5b or ACI 318-11 Eq. D-27, as applicable, need not be taken less than  $c_{Na}/c_{ac}$ . For all other cases,  $\psi_{cp,Na}$  shall be taken as 1.0.

The critical edge distance, cac must be calculated according to Eq. 17.6.5.5.1c for ACI 318-19, Eq. 17.4.5.5c for ACI 318-14 or Eq. D-27a for ACI 318-11, in lieu of ACI 318-19 17.9.5, ACI 318-14 17.7.6 or ACI 318-11 D.8.6, as

$$c_{ac} = h_{ef} \cdot \left(\frac{\tau_{k, uncr}}{1160}\right)^{0.4} \cdot \left[3.1 - 0.7 \frac{h}{h_{ef}}\right]$$

(Eq. 17.6.5.5.1c for ACI 318-19, Eq. 17.4.5.5c for ACI 318-14 or Eq. D-27a for ACI 318-11)

where

$$\left[\frac{h}{h_{ef}}\right]$$
 need not be taken as larger than 2.4; and

 $\tau_{k,uncr}$  = the characteristic bond strength stated in the tables of this report whereby  $\tau_{k,uncr}$  need not be taken as larger

$$au_{k,uncr} = rac{k_{uncr}\sqrt{h_{ef}f_c'}}{\pi \cdot d_a}$$
 Eq. (4-1)

4.1.11 Requirements for Seismic Design Categories C, D, E and F: In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, anchors must be designed in accordance with ACI 318-19 17.10, ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable, except as described below.

The nominal steel shear strength, V<sub>sa</sub>, must be adjusted by  $\alpha_{V,seis}$  as given in Tables 4, 7, 11 and 13 for the corresponding anchor steel. The nominal bond strength  $\tau_{\kappa,cr}$ must be adjusted by  $\alpha_{N,seis}$  as given in Tables 6 and 12 for threaded rods, and Tables 9 and 15 for reinforcing bars.

As an exception to ACI 318-11 Section D.3.3.4.2: Anchors designed to resist wall out-of-plane forces with design strengths equal to or greater than the force determined in accordance with ASCE 7 Equation 12.11-1 or 12.14-10 shall be deemed to satisfy ACI 318-11 Section D.3.3.4.3(d).

Under ACI 318-11 D.3.3.4.3(d), in lieu of requiring the anchor design tensile strength to satisfy the tensile strength requirements of ACI 318-11 D.4.1.1, the anchor design tensile strength shall be calculated from ACI 318-11 D.3.3.4.4.

The following exceptions apply to ACI 318-11 D.3.3.5.2:

1. For the calculation of the in-plane shear strength of anchor bolts attaching wood sill plates of bearing or non-bearing walls of light-frame wood structures to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3 need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:

- 1.1. The allowable in-plane shear strength of the anchor is determined in accordance with AF&PA NDS Table 11E for lateral design values parallel to grain.
- 1.2. The maximum anchor nominal diameter is <sup>5</sup>/<sub>8</sub> inch (16 mm).
- 1.3. Anchor bolts are embedded into concrete a minimum of 7 inches (178 mm).
- 1.4. Anchor bolts are located a minimum of 13/4 inches (45 mm) from the edge of the concrete parallel to the length of the wood sill plate.
- 1.5. Anchor bolts are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the wood sill plate.
- 1.6. The sill plate is 2-inch or 3-inch nominal thickness.
- 2. For the calculation of the in-plane shear strength of anchor bolts attaching cold-formed steel track of bearing or non-bearing walls of light-frame construction to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3 need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:
  - 2.1. The maximum anchor nominal diameter is <sup>5</sup>/<sub>8</sub> inch (16 mm).
  - 2.2. Anchors are embedded into concrete a minimum of 7 inches (178 mm).
  - 2.3. Anchors are located a minimum of 13/4 inches (45 mm) from the edge of the concrete parallel to the length of the track.
  - 2.4. Anchors are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the track.
  - 2.5. The track is 33 to 68 mil designation thickness.

Allowable in-plane shear strength of exempt anchors, parallel to the edge of concrete shall be permitted to be determined in accordance with AISI S100 Section E3.3.1.

3. In light-frame construction, bearing or nonbearing walls, shear strength of concrete anchors less than or equal to 1 inch [25 mm] in diameter attaching a sill plate or track to foundation or foundation stem wall need not satisfy ACI 318-11 D.3.3.5.3(a) through (c) when the design strength of the anchors is determined in accordance with ACI 318-11 D.6.2.1(c).

# 4.2 Strength Design of Post-Installed Reinforcing Bars:

4.2.1 General: The design of straight post-installed deformed reinforcing bars must be determined in accordance with ACI 318 rules for cast-in place reinforcing bar development and splices and this report.

Examples of typical applications for the use of post-installed reinforcing bars are illustrated in Figure 5 of this report.

4.2.2 Determination of bar development length  $I_a$ : Values of I<sub>d</sub> must be determined in accordance with the ACI 318 development and splice length requirements for straight cast-in place reinforcing bars.

### Exceptions:

For uncoated and zinc-coated (galvanized) post-installed reinforcing bars, the factor  $\Psi_e$  shall be taken as 1.0. For all other cases, the requirements in ACI 318-19 25.4.2.5, ACI 318-14 25.4.2.4 or ACI 318-11 12.2.4 (b) shall apply.

2. When using alternate methods to calculate the development length (e.g., anchor theory), the applicable factors for post-installed anchors generally apply.

**4.2.3 Minimum Member Thickness,**  $h_{min}$ , **Minimum Concrete Cover,**  $c_{c,min}$ , **Minimum Concrete Edge Distance,**  $c_{b,min}$ , **Minimum Spacing,**  $s_{b,min}$ : For post-installed reinforcing bars, there is no limit on the minimum member thickness. In general, all requirements on concrete cover and spacing applicable to straight cast-in bars designed in accordance with ACI 318 shall be maintained.

For post-installed reinforcing bars installed at embedment depths,  $h_{ef}$ , larger than 20d ( $h_{ef}$  > 20d), the minimum concrete cover shall be as follows:

REBAR SIZE	MINIMUM CONCRETE COVER, $c_{c,min}$
d <sub>b</sub> ≤ No. 6 (16mm)	1³/ <sub>16</sub> in. (30mm)
No. $6 < d_b \le No.10$	1 <sup>9</sup> / <sub>16</sub> in. (40mm)
$(16mm < d_b \le 32mm)$	1 716 III. (40IIIIII)

The following requirements apply for minimum concrete edge and spacing for  $h_{ef} > 20$ d:

Required minimum edge distance for post-installed reinforcing bars (measured from the center of the bar):

 $c_{b,min} = d_0/2 + c_{c,min}$ 

Required minimum center-to-center spacing between post-installed bars:

 $s_{b,min} = d_0 + c_{c,min}$ 

Required minimum center-to-center spacing from existing (parallel) reinforcing:

 $s_{b,min} = d_b/2$  (existing reinforcing) +  $d_0/2$  +  $c_{c,min}$ 

**4.2.4 Design Strength in Seismic Design Categories C, D, E and F:** In structures assigned to Seismic Category C, D, E or F under the IBC or IRC, design of straight postinstalled reinforcing bars must take into account the provisions of ACI 318-19 Chapter 18, ACI 318-14 Chapter 18 or ACI 318-11 Chapter 21, as applicable.

# 4.3 Installation:

Installation parameters are illustrated in Figure 1 of this report. Installation must be in accordance with ACI 318-19 26.7.2, ACI 318-14 17.8.1 and 17.8.2 or ACI 318-11 D.9.1 and D.9.2. Anchor and post-installed reinforcing bar locations must comply with this report and the plans and specifications approved by the code official. Installation of the IHL OCTOPLATINUM Adhesive Anchor and Post-Installed Reinforcing Bar Systems must conform to the manufacturer's printed installation instructions included in each unit package and provided in Figure 6 of this report.

The adhesive anchor system may be used for upwardly inclined orientation applications (e.g., overhead). Upwardly inclined and horizontal orientation applications are to be installed using piston plugs for the  $^5/_8$ -inch- through  $^{11}/_4$ -inch-diameter (M16 through M30) threaded steel rods and No. 5 through No. 10 (14 mm through 32 mm) steel reinforcing bars, installed in the specified hole diameter, and attached to the mixing nozzle and extension tube supplied by IHL as described in Figure 6 in this report. Upwardly inclined and horizontal orientation installation for the  $^{3}/_8$ -inch- and  $^{1}/_2$ -inch-diameter (M10 and M12) threaded steel rods, and No. 3 and No. 4 (10 mm and 12 mm) steel reinforcing bars may be injected directly to the end of the hole using a mixing nozzle with a bore hole depth  $d_0 \le 10$ " (250 mm).

Installation of anchors in horizontal or upwardly inclined (overhead) orientations shall be fully restrained from movement throughout the specified curing period through the use of temporary wedges, external supports, or other methods. Where temporary restraint devices are used, their use shall not result in impairment of the anchor shear resistance.

# 4.4 Special Inspection:

Periodic special inspection must be performed where required in accordance with Section 1705.1.1 and Table 1705.3 of the 2021, 2018, 2015 and 2012 IBC, 1704.4 and 1704.15 of the 2009 IBC and this report. The special inspector must be on the jobsite initially during anchor or post-installed reinforcing bar installation to verify the anchor or post-installed reinforcing bar type and dimensions, adhesive expiration date, concrete type, concrete compressive strength, hole dimensions, hole cleaning procedures, spacing, edge distances, concrete thickness, anchor or post-installed reinforcing bar embedment, tightening torque, and adherence to the manufacturers printed installation instructions.

The special inspector must verify the initial installations of each type and size of adhesive anchor or post-installed reinforcing bar by construction personnel on site. Subsequent installations of the same anchor or post-installed reinforcing bar type and size by the same construction personnel are permitted to be performed in the absence of the special inspector. Any change in the anchor or post-installed reinforcing bar product being installed or the personnel performing the installation requires an initial inspection. For ongoing installations over an extended period, the special inspector must make regular inspections to confirm correct handling and installation of the product.

Continuous special inspection of adhesive anchors or post-installed reinforcing bars installed in horizontal or upwardly inclined orientations to resist sustained tension loads must be performed in accordance with ACI 318-19 26.13.3.2 (e) and 26.7.1(j), ACI 318-14 17.8.2.4, 26.7.1(h) and 26.13.3.2 (c) or ACI 318-11 D.9.2.4, as applicable.

Under the IBC, additional requirements as set forth in Sections 1705, 1706 or 1707 must be observed, where applicable.

# 4.5 Compliance with NSF/ANSI Standard 61:

The IHL OCTOPLATINUM Adhesive Anchor System complies with the requirements of NSF/ANSI Standard 61, as referenced in Section 605 of the 2021, 2018, 2015, 2012, and 2009 *International Plumbing Code*<sup>®</sup> (IPC) and is certified for use as an anchoring adhesive for installing threaded rods less than or equal to 1.3 inches (33 mm) in diameter in concrete for water treatment applications.

# 5.0 CONDITIONS OF USE

The IHL OCTOPLATINUM Adhesive Anchor System and Post-Installed Reinforcing Bar System described in this report comply with or are a suitable alternative to what is specified in, those codes listed in Section 1.0 of this report, subject to the following conditions:

- 5.1 IHL OCTOPLATINUM adhesive anchors and postinstalled reinforcing bars must be installed in accordance with the manufacturer's printed installation instructions included with each cartridge and provided in Figure 6 of this report.
- 5.2 The anchors and post-installed reinforcing bars described in this report must be installed in cracked and uncracked normalweight concrete having a

- specified compressive strength  $f_c$  = 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).
- **5.3** The concrete shall have attained its minimum specified compressive strength,  $f_c$ , prior to installation of the anchors and post installed reinforcing bars.
- **5.4** The values of  $f_c$  used for calculation purposes must not exceed 8,000 psi (55 MPa). The value of  $f_c$  used for calculation of tension resistance must be limited to 2,500 psi (17.2 MPa) maximum for metric reinforcing bars used as anchorage in cracked concrete only
- 5.5 Anchors and post-installed reinforcing bars must be installed in concrete base materials in holes predrilled in accordance with the instructions provided in Figure 6 of this report.
- 5.6 Loads applied to the anchors and post-installed reinforcing bars must be adjusted in accordance with Section 1605.1 of the 2021 IBC or Section 1605.2 of the 2018, 2015, and 2012 IBC for strength design.
- 5.7 In structures assigned to Seismic Design Categories C, D, E, and F under the IBC or IRC, anchor strength must be adjusted in accordance with Section 4.1.11 of this report, and post-installed reinforcing bars must comply with Section 4.2.4 of this report.
- 5.8 IHL OCTOPLATINUM adhesive anchors and postinstalled reinforcing bars are permitted to be installed in concrete that is cracked or that may be expected to crack during the service life of the anchors and postinstalled reinforcing bars, subject to the conditions of this report.
- 5.9 Strength design values of the post-installed anchors are established in accordance with Section 4.1 of this report.
- 5.10 Post-installed reinforcing bar development and splice lengths are established in accordance with Section 4.2 of this report.
- 5.11 Minimum anchor spacing and edge distance as well as minimum member thickness must comply with the values described in this report.
- 5.12 Post-installed reinforcing bar spacing, minimum member thickness, and cover distance must be in accordance with the provisions of ACI 318 for cast-in place bars and Section 4.2.3 of this report.
- 5.13 Prior to installation of anchors and post-installed reinforcing bars, calculations and details demonstrating compliance with this report must be submitted to the code official. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- 5.14 Anchors and post-installed reinforcing bars are not permitted to support fire-resistive construction. Where not otherwise prohibited by the code, the anchors and post-installed reinforcing bars are permitted for installation in fire-resistive construction provided that at least one of the following conditions is fulfilled:
  - Anchors and post-installed reinforcing bars are used to resist wind or seismic forces only.
  - Anchors and post-installed reinforcing bars that support gravity load-bearing structural elements are within a fire-resistive envelope or a fire-resistive membrane, are protected by approved fire-resistive materials, or have been evaluated for resistance to

- fire exposure in accordance with recognized standards.
- Anchors and post-installed reinforcing bars are used to support non-structural elements.
- 5.15 Since an ICC-ES acceptance criteria for evaluating data to determine the performance of adhesive anchors and post-installed reinforcing bars subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report.
- **5.16** Use of zinc-plated carbon steel threaded rods or steel reinforcing bars is limited to dry, interior locations.
- 5.17 Use of hot-dipped galvanized carbon steel and stainless steel rod is permitted for exterior exposure or damp environments.
- 5.18 Steel anchoring elements in contact with preservative-treated and fire-retardant-treated wood shall be of zinc-coated steel or stainless steel. The minimum coating weights for zinc-coated steel shall be in accordance with ASTM A153.
- 5.19 Periodic special inspection must be provided in accordance with Section 4.4 in this report. Continuous special inspection for anchors and post-installed reinforcing bars installed in horizontal or upwardly inclined orientations to resist sustained tension loads must be provided in accordance with Section 4.4 of this report.
- 5.20 Installation of anchors and post-installed reinforcing bars in horizontal or upwardly inclined orientations to resist sustained tension loads must be performed by personnel certified by an applicable certification program in accordance with ACI 318-19 26.7.2(e), ACI 318-14 17.8.2.2 or 17.8.2.3 or ACI 318-11 D.9.2.2 or D.9.2.3, as applicable.
- 5.21 IHL OCTOPLATINUM adhesive anchors and postinstalled reinforcing bars may be used to resist tension and shear forces in floor, wall for overhead installations into concrete with a temperature between 23°F and 104°F (-5°C and 40°C) for threaded rods and rebar.
- 5.22 Anchors and post-installed reinforcing bars shall not be used for installations where the concrete temperature can vary from 40°F (5°C) or less to 80°F (27°C) or higher within a 12-hour period. Such applications may include but are not limited to anchorage of building facade systems and other applications subject to direct sun exposure.
- 5.23 IHL OCTOPLATINUM adhesive is manufactured under a quality-control program with inspections by ICC-ES.

# **6.0 EVIDENCE SUBMITTED**

Data in accordance with the ICC-ES Acceptance Criteria for Post-Installed Adhesive Anchors in Concrete (AC308), dated June 2019, editorially revised February 2021, which incorporates requirements in ACI 355.4-11 for use in cracked and uncracked concrete; including, but not limited to, tests under freeze/thaw conditions, tests under sustained load, tests for installation including installation direction and condition, tests at elevated temperatures, tests for resistance of alkalinity, tests for resistance to sulphur and tests for seismic tension and shear.

# 7.0 IDENTIFICATION

7.1 IHL OCTOPLATINUM adhesive is identified by packaging labelled with the company's name (Investments Hardware Limited) and address, anchor name, the lot number, the expiration date, and the evaluation report number (ESR-4931). Threaded rods, nuts, washers, and deformed reinforcing bars must be standard steel anchor elements and must conform to applicable national or international specifications as set forth in Tables 2 and 3 of this report.

**7.2** The report holder's contact information is the following:

INVESTMENTS HARDWARE LIMITED 250 ROWNTREE DAIRY ROAD VAUGHAN, ONTARIO L4L 9J7 CANADA (416) 748-0204 www.ihlcanada.com

# **TABLE 1—DESIGN STRENGTH - TABLE REFERENCE INDEX**

DESIGN	STRENGTH1 - TREADED RODS	Fractional	Metric
	Steel Strength - $N_{sa}$ , $V_{sa}$	Table 4	Table 10
	Concrete Strength - $N_{pn}$ , $N_{sb}$ , $N_{sbg}$ , $N_{cb}$ , $N_{cbg}$ , $V_{cb}$ , $V_{cbg}$ , $V_{cp}$ , $V_{cpg}$	Table 5	Table 11
3	Bond Strength <sup>2</sup> - N <sub>a</sub> , N <sub>ag</sub>	Table 6	Table 12
DESIGN S	FRENGTH <sup>1</sup> – REINFORCING STEEL	Fractional	Metric
	Steel Strength - Nsa, Vsa	Table 7	Table 13
THE PROPERTY OF THE PARTY OF TH	Concrete Strength - $N_{pn}$ , $N_{sb}$ , $N_{sbg}$ , $N_{cb}$ , $N_{cbg}$ , $V_{cb}$ , $V_{cbg}$ , $V_{cp}$ , $V_{cpg}$	Table 8	Table 14
	Bond Strength <sup>2</sup> - N <sub>a</sub> , N <sub>ag</sub>	Table 9	Table 15
	Determination of development length for post-installed reinforcing bar connections	Table 16	Table 17

<sup>&</sup>lt;sup>1</sup>Ref. ACI 318-19 17.5.2, ACI 318-14 17.3.1.1 or 318-11 D.4.1.1, as applicable.

# TABLE 2—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON CARBON AND STAINLESS STEEL THREADED ROD MATERIALS1

	THREADED ROD SPECIFICATION		MINIMUM SPECIFIED ULTIMATE STRENGTH, f <sub>uta</sub>	MINIMUM SPECIFIED YIELD STRENGTH 0.2 PERCENT OFFSET, fya	f <sub>uta</sub> /f <sub>ya</sub>	ELONGATION, MIN. PERCENT <sup>11</sup>	REDUCTION OF AREA, MIN. PERCENT	SPECIFICATION FOR NUTS <sup>12</sup>
	ASTM A193 <sup>2</sup> Grade B7	psi (MPa)	125,000 (860)	105,000 (720)	1.19	16	50	ASTM A194 / A563 Grade DH
	ASTM A36 <sup>3</sup> / F1554 <sup>4</sup> , Grade 36	psi (MPa)	58,000 (400)	36,000 (250)	1.61	23	40	ASTM A194 / A563
	ASTM F1554 <sup>4</sup> Grade 55	psi (MPa)	75,000 (515)	55,000 (380)	1.36	23	40	Grade A
TEEL	ASTM F1554 <sup>4</sup> Grade 105	psi (MPa)	125,000 (860)	105,000 (725)	1.19	15	45	
CARBON STEEL	ASTM A449 <sup>5</sup> (3/8" to1" dia.)	psi (MPa)	120,000 (830)	92,000 (635)	1.30	14	35	ASTM A194 / A563 Grade DH
CARE	ASTM A449 <sup>5</sup> (1-1/4" dia.)	psi (MPa)	105,000 (720)	81,000 (560)	1.30	14	35	
	ASTM F568M <sup>6</sup> Class 5.8 (equivalent to ISO 898-1)	psi (MPa)	72,500 (500)	58,000 (400)	1.25	10	35	A563 Grade DH DIN 934 (8-A2K) <sup>13</sup>
	ISO 898-1 <sup>7</sup> Class 5.8	MPa (psi)	500 (72,500)	400 (58,000)	1.25	22	-	EN ISO 4032 Grade 6
	ISO 898-1 <sup>7</sup> Class 8.8	MPa (psi)	800 (118,000)	640 (92,800)	1.25	12	52	EN ISO 4032 Grade 8
	ASTM F593 <sup>8</sup> CW1 <sup>3</sup> / <sub>8</sub> to <sup>5</sup> / <sub>8</sub> in.	psi (MPa)	100,000 (690)	65,000 (450)	1.54	20	-	ASTM F594 Alloy
STEEL	ASTM F593 <sup>8</sup> CW2 <sup>3</sup> / <sub>4</sub> to 1 <sup>1</sup> / <sub>4</sub> in.	psi (MPa)	85,000 (590)	45,000 (310)	1.89	25	-	Group 1, 2 or 3
	ASTM A193/A193M <sup>9</sup> Grade B8/B8M2, Class 2B	psi (MPa)	95,000 (655)	75,000 (515)	1.27	25	40	ASTM A194/A194M
STAINLESS	ISO 3506-1 <sup>10</sup> A4-70 M10-M24	MPa (psi)	700 (101,500)	450 (65,250)	1.56	40	-	EN ISO 4032
	ISO 3506-1 <sup>10</sup> A4-50 M27-M30	MPa (psi)	500 (72,500)	210 (30,450)	2.38	40	-	EN ISO 4032

Adhesive must be used with continuously threaded carbon or stainless steel rod (all-thread) having thread characteristics complying with ANSI B1.1 UNC Coarse **Thread Series** 

<sup>&</sup>lt;sup>2</sup>See Section 4.1.4 of this evaluation report.

<sup>&</sup>lt;sup>2</sup>Standard Specification for Alloy-Steel and Stainless steel Bolting Materials for High temperature of High Pressure service and Other Special Purpose Applications.

<sup>&</sup>lt;sup>3</sup>Standard Specification for Carbon Structural steel.

<sup>-</sup>Standard Specification for Carbon Studential steel.

-Standard Specification for Anchor Bolts, Steel 36, 55 and 105-ksi Yield Strength.

-Standard Specification for Hex Cap Screws, Bolts and Studs, Heat Treated, 120/105/50 ksi Minimum Tensile Strength, General Use.

-Standard Specification for Carbon and Alloy Steel external Threaded Metric Fasteners.

<sup>&</sup>lt;sup>7</sup>Mechanical properties of fasteners made of carbon steel and alloy steel - Part 1: Bolts, Screws and Studs.

<sup>&</sup>lt;sup>8</sup>Standard Specification for Stainless Steel Bolts, Hex Cap Screws, and Studs.
<sup>9</sup>Standard Specification for Alloy-Steel and Stainless Steel Bolting for High Temperature or High Pressure Service and Other Special Purpose Applications.

<sup>&</sup>lt;sup>10</sup>Mechanical properties of corrosion-resistant stainless steel fasteners - Part 1: Bolts, Screws and Studs.

<sup>&</sup>lt;sup>11</sup>Based on 2-in. (50 mm) gauge length except for ASTM A193, which is based on a gauge length of 4d.

<sup>12</sup>Nuts and washers of other grades and style having specified proof load stress greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded rod.

<sup>&</sup>lt;sup>13</sup>Nuts for metric rods.

# TABLE 3—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON STEEL REINFORCING BARS

REINFORCING SPECIFICATION	UNITS	MINIMUM SPECIFIED ULTIMATE STRENGTH, futa	MINIMUM SPECIFIED YIELD STRENGTH, $f_{ya}$
ASTM A615 <sup>1</sup> , A767 <sup>3</sup> , A996 <sup>4</sup>	psi	90,000	60,000
Grade 60	(MPa)	(620)	(414)
ASTM A706 <sup>2</sup> , A767 <sup>3</sup>	psi	80,000	60,000
Grade 60	(MPa)	(550)	(414)
ASTM A615 <sup>1</sup> , Grade 40	psi	60,000	40,000
	(MPa)	(415)	(275)
DIN 488 <sup>5</sup> BSt 500	MPa	550	500
	(psi)	(79,750)	(72,500)

Standard Specification for Deformed and Plain Carbon-Steel Bars for Concrete Reinforcement.

Standard Specification for Low-Alloy Steel Deformed and Plain Bars for Concrete Reinforcement.

Standard specification for Zinc-Coated (Galvanized) steel Bars for Concrete Reinforcement.

Standard specification for Rail-Steel and Axle-steel Deformed bars for Concrete Reinforcement.

Reinforcing steel, reinforcing steel bars; dimensions and masses.

TABLE 4—STEEL DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD1

DE0:0:::	NEGRMATION		11.2	Nominal Rod Diameter (inch)						
DESIGN I	NFORMATION	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	1 <sup>1</sup> / <sub>4</sub>
Threaded	rod O.D.	d	in. (mm)	0.375 (9.5)	0.500 (12.7)	0.625 (15.9)	0.750 (19.1)	0.875 (22.2)	1.000 (25.4)	1.250 (31.8)
Threaded	rod effective cross-sectional area	Ase	in.² (mm²)	0.0775 (50)	0.1419 (92)	0.2260 (146)	0.3345 (216)	0.4617 (298)	0.6057	0.9691 (625)
4,		Nsa	lb	4,495	8,230	13,110	19,400	26,780	35,130	56,210
F155 36	Nominal strength as governed by steel strength (for a single anchor)		(kN) lb	(20.0) 2,695	(36.6) 4,940	(58.3) 7,860	(86.3) 11,640	(119.1) 16,070	(156.3) 21,080	(250.0)
M A36/F Grade 3	Deduction fortes for a signal of the same	V <sub>sa</sub>	(kN)	(12.0)	(22.0)	(35.0)	(51.8)	(71.4)	(93.8)	(150.0)
ي ق	Reduction factor for seismic shear	α <sub>V,seis</sub>	-				0.60			
AST	Strength reduction factor for tension <sup>2</sup>	φ	-				0.75			
`	Strength reduction factor for shear <sup>2</sup>	φ	-		1	1	0.65	1	1	1
4	Nominal strength as governed by steel	N <sub>sa</sub>	lb (kN)	5,815 (25.9)	10,645 (47.6)	16,950 (75.5)	25,090 (111.7)	34,630 (154.1)	45,430 (202.1)	72,685 (323.1)
ASTM F1554 Grade 55	strength (for a single anchor)	V <sub>sa</sub>	lb (kN)	3,490 (15.5)	6,385 (28.6)	10,170 (45.3)	15,055 (67)	20,780 (92.5)	27,260 (121.3)	43,610 (193.9)
TM	Reduction factor for seismic shear	α <sub>V,seis</sub>	-				0.60			
AS	Strength reduction factor for tension <sup>2</sup>	φ	-				0.75			
	Strength reduction factor for shear <sup>2</sup>	φ	-				0.65			
	Nominal strength as governed by steel	N <sub>sa</sub>	lb (kN)	9,685 (43.1)	17,735 (78.9)	28,250 (125.7)	41,810 (186.0)	57,710 (256.7)	75,710 (336.8)	121,135 (538.8)
ASTM A193 Grade B7 ASTM F1554 Grade 105		V <sub>sa</sub>	lb (kN)	5,810 (25.9)	10,640 (47.3)	16,950 (75.4)	25,085 (111.6)	34,625 (154.0)	45,425 (202.1)	72,680 (323.3)
TM M de	Reduction factor for seismic shear	α <sub>V,seis</sub>	- (1014)	0.60						
AST AST G	Strength reduction factor for tension <sup>2</sup>	φ	_	- 0.75						
	Strength reduction factor for shear <sup>2</sup>	φ	-	0.65						
	Strength reduction factor for shear	Ψ	- Ib	9,300	17,030	27,120	40,140	55,405	72,685	101,755
6†	Nominal strength as governed by steel	Nsa	(kN)	(41.4)	(76.2)	(120.9)	(178.8)	(246.7)	(323.7)	(450.0)
ASTM A449	strength (for a single anchor)	V <sub>sa</sub>	lb (kN)	5,580 (24.8)	10,220 (45.7)	16,270 (72.5)	24,085 (107.3)	33,240 (148)	43,610 (194.2)	61,055 (270.0)
STI	Reduction factor for seismic shear	αv,seis	-				0.60			
⋖	Strength reduction factor for tension <sup>2</sup>	$\phi$	-				0.75			
	Strength reduction factor for shear <sup>2</sup>	$\phi$	-				0.65			
>	Nominal strength as governed by steel	N <sub>sa</sub>	lb (kN)	5,620 (25)	10,290 (46)	16,385 (73)	24,250 (108)	33,470 (149)	43,910 (195.5)	70,260 (312.5)
ASTM F568M Class 5.8	strength (for a single anchor)	V <sub>sa</sub>	lb (kN)	3,370 (15)	6,175 (27.6)	9,830 (43.8)	14,550 (64.8)	20,085 (89.4)	26,350 (117.3)	42,155 (187.5)
IM	Reduction factor for seismic shear	αv,seis	-				0.60			
AS	Strength reduction factor for tension <sup>2</sup>	φ	-				0.65			
	Strength reduction factor for shear <sup>2</sup>	φ	-				0.60			
*	Nominal strength as governed by steel	N <sub>sa</sub>	lb (kN)	7,750 (34.5)	14,190 (63.1)	22,600 (100.5)	28,430 (126.5)	39,245 (174.6)	51,485 (229.0)	82,370 (366.4)
F593 CW iinless	strength (for a single anchor)	V <sub>sa</sub>	lb (kN)	4,650 (20.7)	8,515 (37.9)	13,560 (60.3)	17,060 (75.9)	23,545 (104.7)	30,890 (137.4)	49,425 (219.8)
∕l Fŧ tain	Reduction factor for seismic shear	α <sub>V,seis</sub>	-	(=3.7)	(57.0)	(55.5)	0.60	()	()	(= .0.0)
ASTM I Stai	Strength reduction factor for tension <sup>2</sup>	φ	_				0.65			
ά	Strength reduction factor for shear <sup>2</sup>	φ	_				0.60			
_	Carongai reduction actor for shear		- Ib	7,365	13,480	21,470	31,780	43,860	57,540	92,065
ASTM A193/A193M Grade B8/B8M2, Class 2B	Nominal strength as governed by steel strength (for a single anchor)	N <sub>sa</sub>	(kN)	(32.8)	(60.3)	(95.6)	(141.5)	(195.2)	(256.1)	(409.4)
193/A B8/B8 ss 2E		V <sub>sa</sub>	lb (kN)	4,420 (19.7)	8,090 (36.2)	12,880 (57.4)	19,070 (84.9)	26,320 (117.1)	34,525 (153.7)	55,240 (245.6)
⊿ A de ∣ Cla	Reduction factor for seismic shear	α <i>∨,seis</i>	-				0.60			
STI	Strength reduction factor for tension <sup>2</sup>	φ	-				0.75			
ĕ Î	Strength reduction factor for shear <sup>2</sup>	$\phi$	-				0.65			

 $^{1}$ Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.2 and 17.7.1.2b, ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Nuts and washers must comply with requirements for the rod.  $^{2}$ The tabulated value of  $\phi$  applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012 IBC, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 D.4.3, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4.

# TABLE 5—CONCRETE BREAKOUT DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT<sup>1</sup>

DEGICAL INFORMATION	0	11.26			Nomina	al Rod Diamete	er (inch)				
DESIGN INFORMATION	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	1 <sup>1</sup> / <sub>4</sub>		
Effectiveness factor for cracked concrete	K <sub>c,cr</sub>	in-lb (SI)				17 (7)					
Effectiveness factor for uncracked concrete	K <sub>c,uncr</sub>	in-lb (SI)		24 (10)							
Min. anchor spacing	S <sub>min</sub>	in. (mm)	1 <sup>7</sup> / <sub>8</sub> (48)								
Min. edge distance	Cmin	in. (mm)	1 <sup>5</sup> / <sub>8</sub> (41)	1 <sup>3</sup> / <sub>4</sub> (44)	2 (51)	2 <sup>3</sup> / <sub>8</sub> (60)	2 <sup>1</sup> / <sub>2</sub> (64)	2 <sup>3</sup> / <sub>4</sub> (70)	3 <sup>1</sup> / <sub>4</sub> (82)		
		(111111)	,	(44)	For smaller edge distances see Section 4.1.9 of this report.						
Min. member thickness	h <sub>min</sub>	in. (mm)		+ 1 <sup>1</sup> / <sub>4</sub> + 30)			$h_{ef} + 2d_0^3$				
Critical edge distance - splitting (for uncracked concrete) <sup>2</sup>	Cac	-			See Sec	ction 4.1.10 of th	is report.				
Strength reduction factor for tension, concrete failure modes, Condition B <sup>2</sup>	φ	-				0.65					
Strength reduction factor for shear, concrete failure modes, Condition B <sup>2</sup>	φ	-				0.70					

<sup>&</sup>lt;sup>1</sup>Additional setting information is described in Figure 6, installation instructions.

TABLE 6—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1

	DEGIGN INFOR	MATION	0	11.24.		No	minal Ro	od Diam	eter (in	ch)	
	DESIGN INFOR	RMATION	Symbol	Units	3/8	1/2	5/8	3/4	<sup>7</sup> / <sub>8</sub>	1	1 <sup>1</sup> / <sub>4</sub>
Minimum embedm	ent		h <sub>ef,min</sub>	in. (mm)	2 <sup>3</sup> / <sub>8</sub> (60)	2 <sup>3</sup> / <sub>4</sub> (70)	3 <sup>1</sup> / <sub>8</sub> (79)	3 <sup>1</sup> / <sub>2</sub> (89)	3 <sup>1</sup> / <sub>2</sub> (89)	4 (102)	5 (127)
Maximum embedm	nent		h <sub>ef,max</sub>	in. (mm)	7 <sup>1</sup> / <sub>2</sub> (191)	10 (254)	12 <sup>1</sup> / <sub>2</sub> (318)	15 (381)	17 <sup>1</sup> / <sub>2</sub> (445)	20 (508)	25 (635)
Temperature	Characteristic bond s	strength in uncracked concrete	Tk,uncr	psi (N/mm²)	2,600 (17.9)	2,415 (16.6)	2,260 (15.6)	2,140 (14.8)	2,055 (14.2)	2,000 (13.8)	1,990 (13.7)
range A <sup>2,3</sup> :	Characteristic bond s	strength in cracked concrete	Tk,cr	psi (N/mm²)	1,040 (7.2)	1,040 (7.2)	1,110 (7.7)	1,220 (8.4)	1,210 (8.4)	1,205 (8.3)	1,145 (7.9)
Temperature	Characteristic bond s	strength in uncracked concrete	Tk,uncr	psi (N/mm²)	2,265 (15.6)	2,100 (14.5)	1,970 (13.6)	1,865 (12.8)	1,785 (12.3)	1,740 (12.0)	1,730 (11.9)
range B <sup>2,3</sup> :	Characteristic bond s	strength in cracked concrete	T <sub>K</sub> ,cr	psi (N/mm²)	905 (6.2)	905 (6.2)	965 (6.7)	1,060 (7.3)	1,055 (7.3)	1,050 (7.2)	995 (6.9)
Temperature	Characteristic bond s	strength in uncracked concrete	Tk,uncr	psi (N/mm²)	1,630 (11.2)	1,515 (10.4)	1,420 (9.8)	1,345 (9.3)	1,290 (8.9)	1,255 (8.6)	1,250 (8.6)
range C <sup>2,3</sup> :	Characteristic bond s	strength in cracked concrete	Tk,cr	psi (N/mm²)	650 (4.5)	655 (4.5)	695 (4.8)	765 (5.3)	760 (5.2)	755 (5.2)	720 (5.0)
	MAC <sup>4,5</sup> cleaning	Anchor category	-	-	2	2	2	Not			
Dry	WAC * cleaning	Strength reduction factor	$\phi_d$	-	0.55	0.55	0.55		арр	licable	
concrete	CAC <sup>5</sup> or HDB <sup>5</sup>	Anchor category	_	-	1	1	1	1	1	1	1
	cleaning	Strength reduction factor	$\phi_d$	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC <sup>4,5</sup> cleaning	Anchor category	_	-	3	2	2			Not	
Water-saturated	WAC * cleaning	Strength reduction factor	$\phi_{ m ws}$	-	0.45	0.55	0.55		арр	licable	
concrete	CAC⁵ or HDB⁵	Anchor category	-	-	2	2	2	2	2	2	2
	cleaning	Strength reduction factor	φws	-	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water filled balas	CAC cloaning	Anchor category	-	-	3	3	3	3	3	3	3
water-filled fibles	Vater-filled holes CAC cleaning Strength reduction factor				0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction factor fo	or seismic tension		∝N,seis	-				0.95			

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi. For concrete compressive strength,  $f_c$  between 2,500 psi and 8,000 psi, the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2500)^{0.10}$ . See Section 4.1.4 of this report.

<sup>&</sup>lt;sup>2</sup>Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of  $\phi$  applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4.

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 161°F (72°C); Temperature range C: Maximum short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>&</sup>lt;sup>3</sup>Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind, bond strengths may be increased by 23 percent for temperature range C.

<sup>&</sup>lt;sup>4</sup>MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.

MAC: manual air cleaning, see Figure 6. CAC: compressed air cleaning, see Figure 6. HDB: cleaning during drilling action with hollow drill bit system.

# TABLE 7—STEEL DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS 1

DESIGN INFORMATION		Symbol	Units				Nominal	Bar Size			
DESI	JN INFORMATION	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No. 10
Reinfo	orcing bar O.D.	d	in. (mm)	0.375 (9.5)	0.500 (12.7)	0.625 (15.9)	0.750 (19.1)	0.875 (22.2)	1.000 (25.4)	1.125 (28.6)	1.250 (31.8)
	orcing bar effective cross- nal area	A <sub>se</sub>	in.² (mm²)	0.110 (71)	0.200 (129)	0.310 (200)	0.440 (284)	0.600 (387)	0.790 (510)	1.000 (645)	1.270 (819)
(C	Nominal strength as governed by steel strength (for a single	N <sub>sa</sub>	lb (kN)	9,900 (44.0)	18,000 (80.1)	27,900 (124.1)	39,600 (176.0)	54,000 (240.0)	71,100 (316.0)	90,000 (400.0)	114,300 (508.0)
, A99(	strength (for a single anchor)	V <sub>sa</sub>	lb (kN)	5,940 (26.4)	10,800 (48.0)	16,740 (74.5)	23,760 (105.7)	32,400 (144.1)	42,660 (189.8)	54,000 (240.2)	68,580 (305.0)
ASTM A615, A767, A996 Grade 60	Reduction factor for seismic shear	αv,seis	-	0.65							
TM A6	Strength reduction factor for tension <sup>2</sup>	φ	-				0.	0.65			
AS	Strength reduction factor for shear <sup>2</sup>	φ	-			0.60					
	Nominal strength as	N <sub>sa</sub>	lb	8,800	16,000	24,800	35,200	48,000	63,200	80,000	101,600
	governed by	7 V Sa	(kN)	(39.1)	(71.2)	(110.3)	(156.6)	(213.5)	(281.1)	(355.9)	(452.0)
је 60	Nominal strength as governed by steel strength (for a single anchor)	17	lb	5,280	9,600	14,880	21,120	28,800	37,920	48,000	60,960
Grac	,	$V_{sa}$	(kN)	(23.5)	(42.7)	(66.2)	(93.9)	(128.1)	(168.7)	(213.5)	(271.2)
ASTM A706 Grade 60	Reduction for seismic shear	αv,seis					0.	65			
ASTI	Strength reduction factor $\phi$ for tension <sup>2</sup>	φ					0.	75			
	Strength reduction factor $\phi$ for shear <sup>2</sup>	φ					0.	65			
	Nominal strength as governed by steel	Nsa	lb (kN)	6,600 (29.4)	12,000 (53.4)	18,600 (82.7)	26,400 (117.4)				
ade 40	strength (for a single anchor)	V <sub>sa</sub>	lb (kN)	3,960 (17.6)	7,200 (32.0)	11,160 (49.6)	15,840 (70.5)		bars are furni	with ASTM A6 shed only in s	
ASTM A615 Grade 40	Reduction factor for seismic shear	αv,seis	-		0.	65			throug	h No. 6	
ASTM	Strength reduction factor for tension <sup>2</sup>	φ	-				0.	0.65			
`	Strength reduction factor for shear <sup>2</sup>	φ	-				0.	60			

<sup>1</sup>Values provided for common bar material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.2 and Eq. 17.7.1.2b, ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable.

<sup>2</sup>The tabulated value of φ applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012 IBC, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of φ must be determined in accordance with ACI 318-11 D.4.4.

# TABLE 8—CONCRETE BREAKOUT DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1

DECICAL INFORMATION	Ob. a.l	l laste				Nominal	Bar Size			
DESIGN INFORMATION	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No.10
Effectiveness factor for cracked concrete	K <sub>c,cr</sub>	in-lb (SI)					7 7)			
Effectiveness factor for uncracked concrete	K <sub>c,uncr</sub>	inlb. (SI)				_	24  0)			
Min. anchor spacing	S <sub>min</sub>	in. (mm)	1 <sup>7</sup> / <sub>8</sub> (48)	2 <sup>1</sup> / <sub>2</sub> (64)	3 (76)	3 <sup>3</sup> / <sub>4</sub> (95)	4 <sup>1</sup> / <sub>4</sub> (108)	4 <sup>3</sup> / <sub>4</sub> (121)	5 <sup>1</sup> / <sub>4</sub> (133)	5 <sup>7</sup> / <sub>8</sub> (149)
Min. edge spacing	C <sub>min</sub>		1 <sup>5</sup> / <sub>8</sub> (41)	1 <sup>3</sup> / <sub>4</sub> (44)	2 (51)	2 <sup>3</sup> / <sub>8</sub> (60)	2 <sup>1</sup> / <sub>2</sub> (64)	2 <sup>3</sup> / <sub>4</sub> (70)	3 (76)	3 <sup>1</sup> / <sub>4</sub> (82)
		(mm)	( )	(44)	For smaller edge distances see Section 4.1.9 of this report.					
Min. member thickness	h <sub>min</sub>	in. (mm)		+ 1 <sup>1</sup> / <sub>4</sub> + 30)			h <sub>ef</sub> +	2d <sub>0</sub> <sup>3</sup>		
Critical edge spacing – splitting (for uncracked concrete)	Cac	-			Se	e Section 4.1	.10 of this rep	ort.		
Strength reduction factor for tension, concrete failure modes, Condition B <sup>2</sup>	φ	-				0.	65			
Strength reduction factor for shear, concrete failure modes, Condition B <sup>2</sup>	φ	-				0.	70			

<sup>&</sup>lt;sup>1</sup>Additional setting information is described in Figure 6, installation instructions.

TABLE 9—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1

DEGION INFOR	MATION						1	lominal	Bar Size	)		
DESIGN INFOR	MATION		Symbol	Units	No.3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No.10
Minimum embed	dment		h <sub>ef,min</sub>	in. (mm)	2 <sup>3</sup> / <sub>8</sub> (60)	2 <sup>3</sup> / <sub>4</sub> (70)	3 <sup>1</sup> / <sub>8</sub> (79)	3 <sup>1</sup> / <sub>2</sub> (89)	3 <sup>1</sup> / <sub>2</sub> (89)	4 (102)	4 <sup>1</sup> / <sub>2</sub> (114)	5 (127)
Maximum embe	dment		h <sub>ef,max</sub>	in. (mm)	7 <sup>1</sup> / <sub>2</sub> (191)	10 (254)	12 <sup>1</sup> / <sub>2</sub> (318)	15 (381)	17 <sup>1</sup> / <sub>2</sub> (445)	20 (508)	22 <sup>1</sup> / <sub>2</sub> (572)	25 (635)
Temperature	Characteristic bo	ond strength in uncracked concrete	Tk,uncr	psi (N/mm²)	2,200 (15.2)	2,100 (14.5)	2,030 (14.0)	1,970 (13.6)	1,920 (13.2)	1,880 (13.0)	1,845 (12.7)	1,815 (12.5)
range A <sup>2,3</sup> :	Characteristic bo	ond strength in cracked concrete	Tk,cr	psi (N/mm²)	1,090 (7.5)	1,055 (7.3)	1,130 (7.8)	1,170 (8.1)	1,175 (8.1)	1,155 (8.0)	1,140 (7.9)	1,165 (8.0)
Temperature	Characteristic bo	ond strength in uncracked concrete	Tk,uncr	psi (N/mm²)	1,915 (13.2)	1,830 (12.6)	1,765 (12.2)	1,715 (11.8)	1,670 (11.5)	1,635 (11.3)	1,615 (11.1)	1,580 (10.9)
range B <sup>2,3</sup> :	Characteristic bo	ond strength in cracked concrete	Tk,cr	psi (N/mm²)	945 (6.5)	915 (6.3)	980 (6.8)	1,015 (7.0)	1,020 (7.0)	1,005 (6.9)	995 (6.8)	1,010 (7.0)
Temperature	Characteristic bo	ond strength in uncracked concrete	Tk,uncr	psi (N/mm²)	1,380 (9.5)	1,315 (9.1)	1,270 (8.8)	1,235 (8.5)	1,205 (8.3)	1,180 (8.1)	1,155 (8.0)	1,140 (7.8)
range C <sup>2,3</sup> :	Characteristic bo	Tk,cr	psi (N/mm²)	680 (4.7)	660 (4.6)	705 (4.9)	735 (5.1)	735 (5.1)	725 (5.0)	715 (4.9)	730 (5.0)	
	MAC <sup>4,5</sup>	Anchor category	-	-	2	2	2	Not applicable				
Dry	cleaning	Strength reduction factor	Фа	-	0.55	0.55	0.55					
concrete	CAC⁵ or HDB⁵	Anchor category	-	-	1	1	1	1	1	1	1	1
	cleaning	Strength reduction factor	Фа	ı	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC <sup>4,5</sup>	Anchor category	_	1	3	2	2			Not		
Water- saturated	cleaning	Strength reduction factor	φws	-	0.45	0.55	0.55			applicable		
concrete	CAC <sup>5</sup> or HDB <sup>5</sup>	Anchor category	_	-	2	2	2	2	2	2	2	2
	cleaning	Strength reduction factor	φws	-	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water-filled	CAC cleaning	Anchor category	-	-	3	3	3	3	3	3	3	3
holes	holes Strength reduction factor				0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction facto	r for seismic tens	ion	∝N,seis	-	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00

<sup>&</sup>lt;sup>2</sup>Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of  $\phi$  applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012 IBC, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4.  $^{3}d_{0}$  = hole diameter.

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi. For concrete compressive strength  $f_c$  between 2,500 psi and 8,000 psi, tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^{0.10}$ . See Section 4.1.4 of this report.

<sup>2</sup>Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 320°F (160°C),  $(f_c/2,f_c)^{0.00}$ . Short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>3</sup> Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short term loads only, such as wind and seismic, bond strengths may be increased by 23 percent for temperature range C.

<sup>&</sup>lt;sup>4</sup>MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.

MAC: manual air cleaning, see Figure 6. CAC: compressed air cleaning, see Figure 6. HDB: cleaning during drilling action with hollow drill bit system.

# TABLE 10—STEEL DESIGN INFORMATION FOR METRIC THREADED ROD1

DEOLG	NI INFORMATION	0	11.24.				Nominal Rod D	iameter (mm)		
DESIG	INFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30
Thread	ded rod O.D.	d	mm ( in.)	10 (0.39)	12 (0.47)	16 (0.63)	20 (0.79)	24 (0.94)	27 (1.06)	30 (1.18)
	ded rod effective cross- nal area	Ase	mm² ( in.²)	58.0 (0.090)	84.3 (0.131)	157 (0.243)	245 (0.380)	353 (0.547)	459 (0.711)	561 (0.870)
8	Nominal strength as governed by steel strength	N <sub>sa</sub>	kN (lb)	29.0 (6,518)	42.2 (9,473)	78.5 (17,643)	122.5 (27,532)	176.5 (39,668)	229.5 (51,580)	280.5 (63,043)
ass 5.8	(for a single anchor)	V <sub>sa</sub>	kN (lb)	17.4 (3,911)	25.3 (5,684)	47.1 (10,586)	73.5 (16,519)	105.9 (23,801)	137.7 (30,948)	168.3 (37,826)
SO 898-1 Class 5.	Reduction factor for seismic shear	α <sub>V,seis</sub>	-				0.60			
80 S9	Strength reduction factor for tension <sup>2</sup>	φ	-				0.65			
2	Strength reduction factor for shear <sup>2</sup>	φ	-				0.60			
	Nominal strength as	N <sub>sa</sub>	kN (lb)	46.4 (10,428)	67.4 (15,157)	125.6 (28,229)	196 (44,051)	282.4 (63,470)	367.2 (82,528)	448.8 (100,868)
ass 8.8	governed by steel strength (for a single anchor)	V <sub>sa</sub>	kN (lb)	27.8 (6,257)	40.5 (9,094)	75.4 (16,937)	117.6 (26,431)	169.4 (38,082)	220.3 (49,517)	269.3 (60,521)
ISO 898-1 Class 8.	Reduction factor for seismic shear	αv,seis	-				0.60			
SO 898	Strength reduction factor for tension <sup>2</sup>	φ	-				0.65			
	Strength reduction factor for shear <sup>2</sup>	φ	-				0.60			
	Nominal strength as governed by steel strength	N <sub>sa</sub>	kN (lb)	40.6 (9,125)	59 (13,263)	109.9 (24,700)	171.5 (38,545)	247.1 (55,536)	229.5 (51,580)	280.5 (63,043)
-1, steel <sup>3</sup>	(for a single anchor)	V <sub>sa</sub>	kN (lb)	24.4 (5,475)	35.4 (7,958)	65.9 (14,820)	102.9 (23,127)	148.3 (33,322)	137.7 (30,948)	168.3 (37,826)
ISO 3506-1, stainless steel <sup>3</sup>	Reduction factor for seismic shear	α <sub>V,seis</sub>	-				0.60			
ISC A4 sta	Strength reduction factor for tension <sup>2</sup>	φ	-				0.65			
	Strength reduction factor for shear <sup>2</sup>	φ	-				0.60			

<sup>&</sup>lt;sup>1</sup>Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.2 and Eq. 17.7.1.2b, ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Nuts and washers must comply with requirements for the rod.

# TABLE 11—CONCRETE BREAKOUT DESIGN INFORMATION FOR METRIC THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1

DESIGN INFORMATION	Cumbal	l lmita			Nomi	nal Rod Diamete	er (mm)		
DESIGN INFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30
Effectiveness factor for cracked concrete	K <sub>c,cr</sub>	SI (in-lb)				7 (17)			•
Effectiveness factor for uncracked concrete	K <sub>c,uncr</sub>	SI (in-lb)				10 (24)			
Min. anchor spacing	Smin	mm ( in.)	50 (2)		75 (3)	95 (3 <sup>3</sup> / <sub>4</sub> )	115 (4 <sup>1</sup> / <sub>2</sub> )	125 (5)	140 (5 <sup>1</sup> / <sub>2</sub> )
Min. edge distance	C <sub>min</sub>	mm ( in.)	40 (1 <sup>5</sup> / <sub>8</sub> )		50 (2)	60 (2 <sup>3</sup> / <sub>8</sub> )	65 (2 <sup>1</sup> / <sub>2</sub> )	75 (3)	80 (3 <sup>1</sup> / <sub>8</sub> )
		( 111.)		(174)	For s	smaller edge dist	ances, see Secti	on 4.1.9 of this	report.
Min. member thickness	h <sub>min</sub>	mm ( in.)		+ 30 + 1 <sup>1</sup> / <sub>4</sub> )			$h_{ef} + 2d_0^3$		
Critical edge distance - splitting (for uncracked concrete) <sup>2</sup>	Cac	-			See Se	ction 4.1.10 of th	is report.		
Strength reduction factor for tension, concrete failure modes, Condition B <sup>2</sup>	φ	,				0.65			
Strength reduction factor for shear, concrete failure modes, Condition B <sup>2</sup>	φ	-				0.70			

<sup>&</sup>lt;sup>1</sup>Additional setting information is described in Figure 6, installation instructions.

<sup>&</sup>lt;sup>2</sup>The tabulated value of  $\phi$  applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012 IBC, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4. <sup>3</sup>A4-70 Stainless steel (M8-M24); A4-50 Stainless steel (M27-M30).

<sup>&</sup>lt;sup>2</sup>Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of φ applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012 IBC, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of φ must be determined in accordance with ACI 318-11 D.4.4.

 $<sup>^{3}</sup>$   $d_{0}$  = hole diameter.

# TABLE 12—BOND STRENGTH DESIGN INFORMATION FOR METRIC THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1

	DEGION II	UEODIA TION	0	11.24.		N	lominal F	Rod Diam	eter (inch	1)	
	DESIGN II	NFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30
Minimum embe	edment		h <sub>ef,min</sub>	mm ( in.)	60 (2.4)	70 (2.8)	80 (3.1)	90 (3.5)	96 (3.8)	108 (4.3)	120 (4.7)
Maximum emb	aximum embedment  Characteristic bond strength in uncracked concrete			mm ( in.)	200 (7.9)	240 (9.4)	320 (12.6)	400 (15.7)	480 (18.9)	540 (21.3)	600 (23.6)
Temperature	emperature		Tk,uncr	N/mm² (psi)	17.7 (2,571)	16.9 (2,453)	15.6 (2,256)	14.6 (2,112)	13.9 (2,020)	13.7 (1,985)	13.7 (1,980)
range A <sup>2,3</sup> :	emperature		Tk,cr	N/mm² (psi)	7.2 (1,039)	7.2 (1,043)	7.7 (1,110)	8.4 (1,217)	8.3 (1,209)	8.3 (1,204)	7.9 (1,149)
Temperature	Characteristic bon	d strength in uncracked concrete	Tk, uncr	N/mm² (psi)	15.4 (2,237)	14.7 (2,134)	13.5 (1,963)	12.7 (1,837)	12.1 (1,757)	11.9 (1,727)	11.9 (1,723)
range B <sup>2,3</sup> :	Characteristic bon	d strength in cracked concrete	Tk,cr	N/mm² (psi)	6.2 (904)	6.3 (908)	6.7 (966)	7.3 (1,058)	7.2 (1,052)	7.2 (1,047)	6.9 (999)
Temperature	Characteristic bon	d strength in uncracked concrete	Tk,uncr	N/mm² (psi)	11.1 (1,612)	10.6 (1,538)	9.8 (1,415)	9.1 (1,324)	8.7 (1,266)	8.6 (1,245)	8.6 (1,241)
range C <sup>2,3</sup> :	Characteristic bon	d strength in cracked concrete	Tk,cr	N/mm² (psi)	4.5 (651)	4.5 (654)	4.8 (696)	5.3 (763)	5.2 (758)	5.2 (755)	5.0 (720)
	MAC <sup>4,5</sup> cleaning	Anchor category	-	-	2	2	2			ot	
Dry	WAC ** cleaning	Strength reduction factor	фа	-	0.55	0.55	0.55		appli	cable	
concrete	CAC <sup>5</sup> or HDB <sup>5</sup>	Anchor category	_	1	1	1	1	1	1	1	1
	cleaning	Strength reduction factor	фа	1	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC4.5 cleaning	Anchor category	_	-	3	2	2			ot	
Water- saturated	Water- MAC <sup>4,5</sup> cleaning Strength reduction factor			-	0.45	0.55	0.55		appli	cable	
concrete	CAC <sup>5</sup> or HDB <sup>5</sup>	Anchor category	-	-	2	2	2	2	2	2	2
	cleaning Strength reduction factor		φws	-	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water-filled	rater-filled CAC cleaning Anchor category			1	3	3	3	3	3	3	3
holes	CAC cleaning 5 3			1	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction fact	or for seismic tensi	on	<i>⋈</i> N,seis	-				0.95			

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi. For concrete compressive strength,  $f_c$  between 2,500 psi and 8,000 psi, the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2500)^{0.10}$ . See Section 4.1.4 of this report.

# TABLE 13—STEEL DESIGN INFORMATION FOR METRIC REINFORCING BARS 1

DECK	ON INCODMATION	0	l luita				Nominal	Bar Size			
DESIG	ON INFORMATION	Symbol	Units	ø 10	ø 12	ø 14	ø 16	ø 20	ø 25	ø 28	ø 32
Reinfo	orcing bar O.D.	d	mm ( in.)	10 (0.394)	12 (0.472)	14 (0.551)	16 (0.630)	20 (0.787)	25 (0.984)	28 (1.102)	32 (1.260)
	orcing bar effective cross- nal area	Ase	mm² ( in.²)	78.5 (0.112)	113.1 (0.175)	153.9 (0.239)	201.1 (0.312)	314.2 (0.487)	490.9 (0.761)	615.8 (0.954)	804.2 (1.247)
	Nominal strength as governed by steel	N <sub>sa</sub>	kN (lb)	43.2 (9,739)	62.2 (14,024)	84.7 (19,088)	110.6 (24,932)	172.8 (38,956)	270.0 (60,868)	338.7 (76,353)	442.3 (99,727)
200	strength (for a single anchor)	V <sub>sa</sub>	kN (lb)	25.9 (5,843)	37.3 (8,414)	50.8 (11,453)	66.4 (14,959)	103.7 (23,373)	162.0 (36,521)	203.2 (45,812)	265.4 (59,836)
38 BSt	Reduction factor for seismic shear	αv,seis	-				0.	65			
DIN 488	Strength reduction factor for tension <sup>2</sup>	φ	-				0.	65			
	Strength reduction factor for shear <sup>2</sup>	φ	-				0.	60			

<sup>&</sup>lt;sup>1</sup>Values provided for common bar material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.2 and Eq. 17.7.1.2b, ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable.

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 161°F (72°C); Temperature range C: Maximum short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>&</sup>lt;sup>3</sup>Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind, bond strengths may be increased by 23 percent for temperature range C.

<sup>4</sup>MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.

<sup>&</sup>lt;sup>5</sup>MAC: manual air cleaning, see Figure 6. CAC: compressed air cleaning, see Figure 6. HDB: cleaning during drilling action with hollow drill bit system.

<sup>&</sup>lt;sup>2</sup>The tabulated value of φ applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012 IBC, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of φ must be determined in accordance with ACI 318-11 D.4.4.

# TABLE 14—CONCRETE BREAKOUT DESIGN INFORMATION METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1

DECICAL INFORMATION	Ob. a.l	Haita				Nom	inal Bar Size				
DESIGN INFORMATION	Symbol	Units	ø 10	Ø 12	ø 14	ø 16	Ø 20	Ø 25	ø 28	ø 32	
Effectiveness factor for cracked concrete	K <sub>c,cr</sub>	SI (in-lb)					7 (17)				
Effectiveness factor for uncracked concrete	K <sub>c,uncr</sub>	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
Min. anchor spacing	Smin			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					150 (5 <sup>7</sup> / <sub>8</sub> )		
Min. edge spacing	Cmin									85 (3 <sup>1</sup> / <sub>8</sub> )	
		( 111.)	( -,	(174)	$ \begin{array}{c ccccc} 60 & 70 & \\ (2^{3}/_{8}) & (2^{3}/_{4}) & \\ 45 & 50 & \\ (1^{3}/_{4}) & & & For \\ /_{4} & & & & \\ 0) & & & & & \\ \end{array} $	or smaller e	dge distances, s	ee Section 4.1	.9 of this repo	ort.	
Min. member thickness	h <sub>min</sub>			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
Critical edge spacing – splitting (for uncracked concrete) <sup>2</sup>	Cac	-				See Section	4.1.10 of this re	port.			
Strength reduction factor for tension, concrete failure modes, Condition B <sup>2</sup>	φ	-									
Strength reduction factor for shear, concrete failure modes, Condition B <sup>2</sup>	φ	-					0.70				

<sup>&</sup>lt;sup>1</sup>Additional setting information is described in Figure 6, installation instructions.

# TABLE 15—BOND STRENGTH DESIGN INFORMATION METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1

DEGIGN INFOR	MATION							Nominal	Bar Size	,		
DESIGN INFORM	WATION		Symbol	Units	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Minimum embed	ment		h <sub>ef,min</sub>	mm ( in.)	60 (2.4)	70 (2.8)	75 (3.0)	80 (3.1)	90 (3.5)	100 (3.9)	112 (4.4)	128 (5.0)
Maximum embed	lment		h <sub>ef,max</sub>	mm ( in.)	200 (7.9)	240 (9.4)	280 (11.0)	320 (12.6)	400 (15.7)	500 (19.7)	560 (22.0)	640 (25.2)
Temperature	Characteristic bond strength in uncracked concrete range A <sup>2,3</sup> :		Tk,uncr	N/mm² (psi)	15.1 (2,183)	14.6 (2,121)	14.0 (2,025)	14.0 (2,025)	13.5 (1,954)	13.0 (1,886)	12.8 (1,852 )	12.5 (1,813 )
range A <sup>2,3</sup> :			Tk,cr	N/mm² (psi)	7.5 (1,082)	7.3 (1,060)	7.9 (1,144)	8.2 (1,193)	8.2 (1,188)	8.0 (1,158)	7.9 (1,144 )	8.0 (1,163 )
Temperature	Characteristic b	ond strength in uncracked concrete	Tk,uncr	N/mm² (psi)	13.1 (1,899)	12.7 (1,845)	12.1 (1,762)	12.1 (1,762)	11.7 (1,700)	11.3 (1,640)	11.1 (1,611 )	10.9 (1,577 )
range B <sup>2,3</sup> :	Characteristic b	ond strength in cracked concrete	Tk,cr	N/mm² (psi)	6.5 (942)	6.4 (922)	6.9 (996)	7.2 (1,038)	7.1 (1,034)	6.9 (1,008)	6.9 (995)	7.0 (1,012 )
Temperature range C <sup>2,3</sup> :	Characteristic b	ond strength in uncracked concrete	Tk,uncr	N/mm² (psi)	9.4 (1,369)	9.2 (1,329)	8.8 (1,270)	8.8 (1,270)	8.4 (1,225)	8.2 (1,182)	8.0 (1,161 )	7.8 (1,136 )
range C	Characteristic b	ond strength in cracked concrete	$ au_{k,cr}$	N/mm² (psi)	4.7 (678)	4.6 (665)	4.9 (718)	5.2 (748)	5.1 (745)	5.0 (726)	4.9 (717)	5.0 (729)
	MAC <sup>4,5</sup>	Anchor category	-	-	2	2	2	2		N		
Dry	cleaning	Strength reduction factor	$\phi_{d}$	-	0.55	0.55	0.55	0.55		Applio	cable	
concrete	CAC⁵ or HDB⁵	Anchor category	-	-	1	1	1	1	1	1	1	1
	cleaning	Strength reduction factor	фа	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC <sup>4,5</sup>	Anchor category	-	-	3	2	2	2		N		
Water-saturated	Nater-saturated cleaning Strength reduction factor		$\phi_{ m ws}$	-	0.45	0.55	0.55	0.55		Applio	cable	
concrete	concrete CAC <sup>5</sup> or HDB <sup>5</sup> Anchor category		-	-	2	2	2	2	2	2	2	2
	cleaning	Strength reduction factor	<i>φ</i> ws	ı	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water-filled	CAC cleaning	Anchor category	_	-	3	3	3	3	3	3	3	3
holes	CAC cleaning		φwf	1	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction factor	CAC cleaning		∝N,seis	-	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi. For concrete compressive strength  $f_c$  between 2,500 psi and 8,000 psi, tabulated characteristic bond strength may not be increased. See Section 4.1.4 of this report.

<sup>&</sup>lt;sup>2</sup>Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of  $\phi$  applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015 and 2012 IBC, ACI 318-19 5.3, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4.  $^3d_0$  = hole diameter.

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 161°F (72°C); Temperature range C: Maximum short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>3</sup>Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short term loads only, such as wind and seismic, bond strengths may be increased by 23 percent for temperature range C.

<sup>4</sup>MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.

TABLE 16—DEVELOPMENT LENGTH FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1, 2, 4

	_	Critoria Section					Bar	size			
DESIGN INFORMATION	Symbol	of Reference Standard	Units	#3	#4	#5	#6	#7	#8	#9	#10
Nominal	,	AOTM A045/A700	in.	0.375	0.500	0.625	0.750	0.875	1.000	1.125	1.250
reinforcing bar diameter	d₅	ASTM A615/A706	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	(28.6)	(31.8)
		A O TAM A O 4 5 / A 7 0 0	in <sup>2</sup>	0.11	0.20	0.31	0.44	0.60	0.79	1.00	1.27
Nominal bar area	A <sub>b</sub>	ASTM A615/A706	(mm²)	(71.3)	(126.7)	(197.9)	(285.0)	(387.9)	(506.7)	(644.7)	(817.3)
Development length for $f_y = 60$		ASTM A615/A706  ASTM A615/A706  ACI 318-19 25.4.2.4 or ACI 318-14 25.4.2.3 or ACI 318-11 12.2.3  ACI 318-19 25.4.2.4 or	in.	12.0	14.4	18.0	21.6	31.5	36.0	40.5	45.0
ksi and $f_c = 2,500$ psi (normalweight concrete) <sup>3</sup>	la	ASTM A615/A706  ACI 318-19 25.4.2.4 or ACI 318-11 12.2.3  ACI 318-11 12.2.3  ACI 318-19 25.4.2.4 or ACI 318-14 25.4.2.3 or	(mm)	(304.8)	(365.8)	(457.2)	(548.6)	(800.1)	(914.4)	(1028.7)	(1143)
Development length for $f_V = 60$			in.	12.0	12.0	14.2	17.1	24.9	28.5	32.0	35.6
ksi and $f'_c$ = 4,000 psi (normalweight concrete) <sup>3</sup>	I <sub>d</sub>	ASTM A615/A706  ACI 318-19 25.4.2.4 or ACI 318-14 25.4.2.3 or ACI 318-11 12.2.3  ACI 318-19 25.4.2.4 or ACI 318-14 25.4.2.3 or	(mm)	(304.8)	(304.8)	(361.4)	(433.7)	(632.5)	(722.9)	(812.8)	(904.2)

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

$${}^{4}\left(\frac{c_{b} + K_{tr}}{d_{b}}\right) = 2.5, \ \psi_{1} = 1.0, \ \psi_{2} = 1.0, \ \psi_{3} = 0.8 \text{ for } d_{b} \le \#6, \ 1.0 \text{ for } d_{b} > \#6.$$

# TABLE 17—DEVELOPMENT LENGTH FOR EU METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR IHL HOLLOW CARBIDE DRILL BIT 1, 2, 4

	_	Critoria Section of	_				Bar size			
DESIGN INFORMATION	Symbo	Reference Standard	Units	8	10	12	16	20	25	32
Nominal reinforcing		50 ///0 0005	mm	8	10	12	16	20	25	32
bar diameter	đь	BS 4449: 2005	(in.)	(0.315)	(0.394)	(0.472)	(0.630)	(0.787)	(0.984)	(1.260)
			mm <sup>2</sup>	50.3	78.5	113.1	201.1	314.2	490.9	804.2
Nominal bar area	A <sub>b</sub>	BS 4449: 2005	(in²)	(80.0)	(0.12)	(0.18)	(0.31)	(0.49)	(0.76)	(1.25)
Development length for $f_y = 72.5$ ksi and		mm	305	348	417	556	871	1087	1392	
f'c = 2,500 psi (normalweight concrete) <sup>3</sup>	I <sub>d</sub>	25.4.2.3 or	(in.)	(12.0)	(13.7)	(16.4)	(21.9)	(34.3)	(42.8)	(54.8)
Development length for $f_y = 72.5$ ksi and			mm	305	305	330	439	688	859	1100
$f_c = 4,000 \text{ psi}$ (normalweight concrete) <sup>3</sup>	la	25.4.2.3 or	(in.)	(12.0)	(12.0)	(13.0)	(17.3)	(27.1)	(33.8)	(43.3)

For **SI**: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

$${}^{4}\left(\frac{c_{b}+K_{tr}}{d_{b}}\right)=2.5$$
,  $\psi_{f}=1.0$ ,  $\psi_{e}=1.0$ ,  $\psi_{b}=0.8$  for  $d_{b}<20$ mm,  $1.0$  for  $d_{b}\geq20$ mm.

<sup>&</sup>lt;sup>5</sup>MAC: manual air cleaning, see Figure 6. CAC: compressed air cleaning, see Figure 6. HDB: cleaning during drilling action with hollow drill bit system.

<sup>&</sup>lt;sup>1</sup> Development lengths valid for static, wind, and earthquake loads (SDC A and B).

<sup>&</sup>lt;sup>2</sup> Development lengths in SDC C through F must comply with ACI 318-19 Chapter 18, ACI 318-14 Chapter 18 or ACI 318-11 Chapter 21 and Section 4.2.4 of this report

 $<sup>^3</sup>$   $f_v$  and  $f_c$  used in this table are for example purposes only. For sand-lightweight concrete, increase development length by 33%, unless the provisions of ACI 318-19 25.4.2.5, ACI 318-14 25.4.2.4 or ACI 318-11 12.2.4 (d) are met to permit  $\lambda > 0.75$ .

<sup>&</sup>lt;sup>1</sup>Development lengths valid for static, wind, and earthquake loads (SDC A and B).

<sup>&</sup>lt;sup>2</sup> Development lengths in SDC C through F must comply with ACI 318-19 Chapter 18, ACI 318-14 Chapter 18 or ACI 318-11 Chapter 21 and Section 4.2.4 of this report.

 $<sup>^3</sup>$   $f_y$  and  $f_c$  used in this table are for example purposes only. For sand-lightweight concrete, increase development length by 33%, unless the provisions of ACI 318-19 25.4.2.5, ACI 318-14 25.4.2.4 or ACI 318-11 12.2.4 (d) are met to permit  $\lambda > 0.75$ .

<sup>&</sup>lt;sup>5</sup> I<sub>d</sub> must be increased by 9.5% to account for ψg in ACI 318-19 25.4.2.4. ψg has been interpolated from Table 25.4.2.5 of ACI 318-19 for fy = 72.5 ksi.

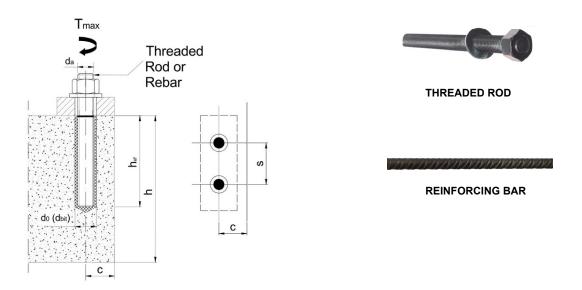


FIGURE 1—INSTALLATION PARAMETERS FOR THREADED RODS AND REINFORCING BARS



FIGURE 2—OCTOPLATINUM ADHESIVE ANCHOR SYSTEM

Drilling and cleaning	Tool	Accessories and Shrouds	Vacuum
Dust extraction system for standard drilling and cleaning equipment		SDS-Plus and SDS-Max Drill Bit  Capture Device ITM# 31816	Dust Extractor
IHL hollow drill bit system	Rotary Drill Hammer	Duster Expert SDS-Plus and SDS-Max Hollow Drill Bit	Class M vacuum with a minimum air flow rating of 90cfm (150m³/h resp. 42l/s).

FIGURE 3—IHL DUST REMOVAL DRILLING SYSTEM WITH HEPA DUST EXTRACTOR OPTIONS

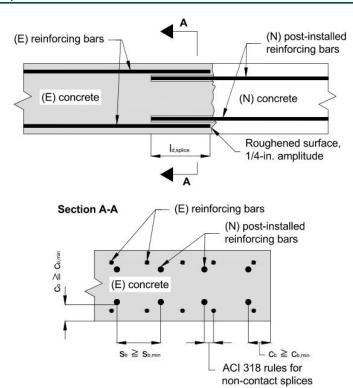


FIGURE 4—INSTALLATION PARAMETERS FOR POST-INSTALLED REINFORCING BARS

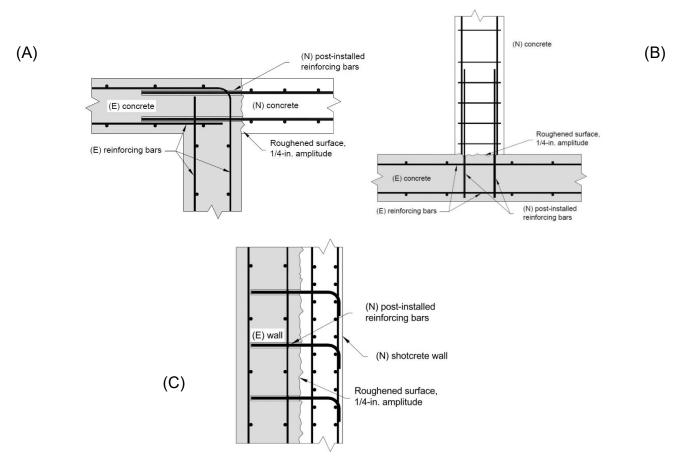


FIGURE 5—APPLICATION EXAMPLES FOR POST-INSTALLED REINFORCING BARS:
(A) TENSION LAP SPLICE WITH EXISTING FLEXURAL REINFORCEMENT; (B) TENSION DEVELOPMENT OF COLUMN DOWELS;
(C) DEVELOPMENT OF SHEAR DOWELS FOR NEWLY THICKENED SHEAR WALL

Drilling

Step 2a for MAC or CAC hole cleaning instructions.

hole (e.g. vacuum, compressed air, etc.) prior to cleaning

case of standing water in the drilled hole, all the water has to be removed from the

the vacuum must be on!) no further cleaning is required → go to Step 3, otherwise to Expert drill bits and a Class M vacuum with air flow 150m³/h resp. 42l/s resp. 90cfm

carbide drill bit must meet the requirements of ANSI Standard B212.15.
For bore holes drilled with the IHL hollow drill bit system (consisting of Heller Duster

# **INUM** - Instruction Card

# Hole cleaning Preparing CAC: Cleaning for all bore hole diameter in uncracked and cracked concrete 4 2c. 2a. ç.v 2c. 2b. 2a. 2b.

be used.

Determine brush diameter (see Table 3) for the drilled hole.

Brush the hole with the

e.g.

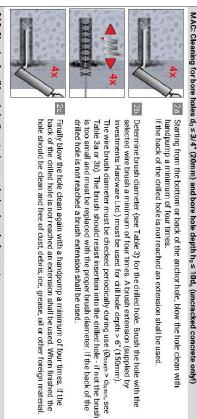
any load (see Table 2)

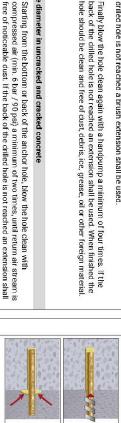
9

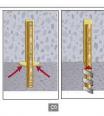
Allow the achesive anchor to cure to the specified full curing time prior to applying

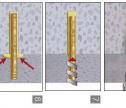
Do not disturb, torque or load the anchor until it is fully cured

selected wire brush a minimum of two times (2x). A brush extension (supplied by

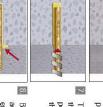


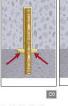












to the anchor may be performed during the gel time but the anchor shall not be secured from moving/falling during the cure time (e.g. wedges). Minor adjustments applications and applications between horizontal and overhead the anchor must be enough adhesive in the hole, the installation must be repeated. For overhead adhesive has flowed from the hole and all around the top of the anchor. If there is not Be sure that the anchor is fully seated at the bottom of the hole and that some

Curing and fixture OE:00 10.

> After full curing of the adhesive anchor, a fixture can be installed to the anchor and tightened up to the maximum torque (shown in Table 4) by using a calibrated torque

Take care not to exceed the maximum torque for the selected anchor

# Gel (working) times and curing times

°C)       10 min       1 h         °C)       6 min       40 min         °C)       3 min       30 min         °C)       2 min       30 min	(+14°C) (+19°C) (+29°C) (+40°C)	67°F 85°F 104°F	ಕ ಕ ಕ	(+15°C) to (+20°C) to (+30°C) to	86 F
10 min ) 6 min ) 3 min	(+14°C) (+19°C) (+29°C)	67°F	ಕ ಕ	(+15°C) (+20°C)	59°F
10 min 6 min	(+14°C) (+19°C)	67°F	<b>♂</b>	(+15°C)	59°F
	(+14°C)	1 00		1/	1 00
	1	ů, œ	₹	(+10°C)	ų V
°C)   15 min   2 h	(+9°C)	49°F	₽	(+5°C)	41 °F
°C)   25 min   3.5 h	(+4°C)	40 °F	₫	(0°C)	32°F
'C)   50 min   5 h	(-1 °C)	31°F	to	(-5°C)	23°F
Gel (working) time Full curing time	rial	ase mate	e of b	Temperature of base material	_

embedment depth has to be marked on the anchor. Verify anchor element is straight Prior to inserting the anchor rod or rebar into the filled drilled hole, the position of the cartridge temperature see Table 2. Attach a supplied mixing nozzle to the cartridge. Do not modify the mixer in any way and make sure the mixing element is inside the Check adhesive expiration date on cartridge label. Do not use expired product. Review

dhesive and also for all work

Safety Data Sheet (SDS) before use. For the permitted range of the base material and

hole is not reached an extension shall be used. When finished the hol dean and free of dust, debris, ice, grease, oil or other foreign material

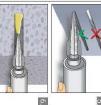
Finally blow the hole clean again with compressed air (min. 6 bar / 90 psi) a minimum small and must be replaced with the proper brush diameter. If the back of the drilled or 3b). The brush should resist insertion into the drilled hole - if not the brush is too brush diameter must be checked periodically during use (Øbrush > dbmin, see Table 3a Investments Hardware Ltd.) must be used for drill hole depth > 6" (150mm). The wire

hole is not reached a brush extension shall be used

of two times, until return air stream is free of noticeable dust. If the back of the drilled

When finished the hole should be

1. Setting instructions for solid base material - For any application not covered by this document please contact Investments Hardware Ltd. (ESR-4931)



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ÇT)

strokes of adhesive through the mixing nozzle until the adhesive is a consistent gray color. Review and note the published working and cure times (see Table 2) prior to Adhesive must be properly mixed to achieve published properties. dispensing adhesive into the drilled hole, separately dispense at least three full

Prior to

case of using the extension tube VL16/1,8 (ITM#33514), cut the tip of the mixer not reached with the mixing nozzle only an extension tube supplied by Investments Hardware Ltd. (ITM# 31412 or ITM# 33514) must be used with the mixing nozzle. Fill the cleaned hole approximately two-thirds full with mixed adhesive starting from fills to avoid creating air pockets or voids. If the bottom or back of the anchor hole is the bottom or back of the anchor hole. Slowly withdraw the mixing nozzle as the hole

nozzle at position "X"

Piston plugs (see Table 3a or 3b) must be used with and attached to mixing nozzle

Insert piston plug to the back of the drilled hole and inject as described in the method with anchor rod 5/8" to 1-1/4" (M16 to M30) diameter and rebar sizes #5 to #10 ( 14 all installations with drill hole depth d, >10" (250mm) overhead installations and installations between horizontal and overhead

above. During installation the piston plug will be naturally extruded from the drilled

Attention! Do not install anchors overhead or

Installation

×

with piston plug:

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positive distribution of the adhesive until the embedment depth is reached. Observe the gel (working) time. The anchor should be free of dirt, grease, oil or other foreign material. Push clean threaded rod or reinforcing bar into the anchor hole while turning slightly to ensure proper training and/or certification. Contact IHL for details prior to use upwardly inclined without installation hardware supplied by IHL and also receiving

	28 fl. oz. l'dispensers	Injection tools 10 fl. oz. dispenser	5. OCTOPL	$h_{ef,max}$ = Maximum embedment (PIR) $s_{mn} = 5xd_s$ . $\Im$ for ASTIN	h <sub>dmin</sub> = Minimum embedment	hmin = Minimum member thickness	c <sub>min</sub> = Min. edge dis	S <sub>min</sub> = Min. spacing	h <sub>of,max</sub> = Maximum embedment	T <sub>max</sub> = Maximum lorque	Parameter valid for anchors	$d_o(d_{DR})$ = Nominal ANSI drill bit size	d <sub>s</sub> = Nominal anchor rod diameter	Anct		4. Anchor p		1-1/4" #9		3/4" #6	#5	5/8" #4	1/2"	- #3		[inch] [inch]	Threaded Rebar		sa. Parame
	ITM #33520 - Pneumatic tool	ΠΜ#3 <b>1534</b> - Manua tool ΠΜ#3 <b>0204 -</b> Pneumatic tool		embedment (PIR) xd <sub>s</sub> . ② for ASTM 36 an	h <sub>drain</sub> = Minimum embedment	mber thickness	$c_{mh}$ = Min. edge distance with 45% $T_{mox}^{(1)}$	tance with 100% T	embedment	rque	anchors	ANSI drill bit size	or rod diarrieter	Anchor size		4. Anchor property / Setting information (fractional and metric sizes		13/8			3/4	11,/16		1/2		(provide	d₀ Drillbit Ø		sa. Parameter cleaning and setting tools (tractional sizes)
2 Ir	OCTOPLATINUM 28 fl. oz.	Cartridge system  OCTOPLATINUM  '0 fl. oz.	sive anchor sy	Iment (PIR)  2) for ASTM 36 and F1554 Grade 36, T <sub>rox</sub> = 11 ftlb		h <sub>er</sub> + 1 1/4	Hf	_	10	15 <sup>2)</sup> 30 44	1 1	9/16	0.500	3/8" 1/2" 5/8"	Nominal threaded rod	information (fr		38.2 1.504			+	20.0 0.787		14.3 0.562	2.10	[mm] [inch]	d₀ Brush ∅	2000 Section 1	secung cools (r
Investments Hardware Limited 250 Rowntree Dairy Road Vaughan, Ontario L4L 9J7, Canada	OCTOPLATINUM mixing nozzle m #33313	tem Extra mixing nozzles	stem and acc	<sub>rax</sub> = 11 ftlb.	9	$h_{ef} + 2d_e$	1.75	4-1/4 2-1/2	15 17-7/2	66 96 147		7/8 1	0.750	inch; ftlb.	eaded rod (fractional)	actional and me		35.8 1.410			-	18.0 0.500		13.2 0.520		[mm] [inch]	d <sub>b,nin</sub> min. Brush <i>Ø</i>		racuollal sizes)
re Limited Road _9J7, Canada	(ITM# Table 3a or 3b)	Piston Plug	essories			h <sub>er</sub> + 30	2.75	5-7/8 50 3-1/4 45	200	221 20 40		1-3/8 12	· .250 10	1-1/4" M10 M12		etric sizes)		0 31436		H		9 31431		0 31428	8 31427	ı E	TM#	<i>"</i>	
www.IHLCanada.com P: +1 416-748-0204	Compressed air nozzle (min. 90 psi)  Tab) If the bore hole ground is not reached an extension shall be used.	Handpump (ITM #31417)		8	ī	h <sub>ef</sub> + 2	45	3 80	320 400	80 120 170 80 co 06		18 22 28	16 20	mm; Nm	Nominal threaded rod (metric)			1 3/8 31447				11/16 31449	No binds reduited	No phase required		(No.) [-]	Piston ITM#		
om 4 [Rev. e]				2		2 <b>d</b> <sub>o</sub>	70	135 150	540 600	250 300		30 35	27	M27 M30	netric)			M30	M27	M24	M20	,	M16	M12	M10	[mm]	Threaded Rod		SD. Fale
<u></u>	Extension tube VL16/1,8  (ITM#33514)	Extension tube VL10/0,75  (ITM #31412)		30 37	2-3/8 2-3/4 3-1/8	h <sub>er</sub> + 1 1/4	H		10	15 <sup>2)</sup> 30 44	1 1	5/8	1/2	#3 #4 #5	Reinfo			25 32	- 30	20 25			12 16			[mm] [mm]	Rebar Drill bit		Sp. Palallietel Clealli
	Brush extension	Extension with wood handle []		52 1/2		$h_{ef} + 2d_o$	75	3-5/8 4-1/4 4-3/4	15 17-1/2	66 96 147 3-1/2 3-1/2 /		7/8 1 1-1/8		inch; ftlb.	Reinforcing bar (fractional)		43.5	34		30				15.5		] [mr	d <sub>տ</sub> Brush		ig and security
28 11. 02.	10 fl. oz.  28 fl. oz.  28 fl. oz.	Cartridge	6. Post	67 · /2 75	4-1/2		$\Box$	5-1/4 5-7/8	22-1/2 25	185 221 4-1/2 5		1-3/8 1-1/2	1-1/8 1-1/4	#9 #10	ıal)		Н	1.34 32.5	1.25 30			0.87 20.5	0.69 16.5		2212	[inch] [r	0	, American	ing and secund cools (injectic sizes)
	umatic umatic		-installed re	720	60 70 75	<b>h</b> <sub>ef</sub> + 30	Н	60	240	20 40 45 60 70 75		14 16 18	12	Ø10 Ø12 Ø·4	Rein:			-	5 1.12	+	H	$\dashv$	5 0.57	H	Н	]	d <sub>ետiո</sub> min. Brush 🗭		sizes)
s 32 ≤ 1920 [mm] [mm] ≤ 1920 [mm]	AI AI AI AI	d <sub>s</sub> h <sub>ef</sub> = #5  2 #5  2 27-1/2 [inch]  5 700 [mm]	Post-installed rebar hef ≥ 20d	960 1200	001 00 08	$h_{ef} + 2d_o$	45		400	80 120 175		20 25 32	16 20	mm; Nm ∅ 16   ∅ 20   ∅ 25	Reinforcing bar (metric)		H	+	31436 VS30	33508 VS 25	H	33506 VS 20	33505 31439 VS 18			[-] (No.)	ITM # Piston		
(ITM#33514)		Extension tube ป VL10/0,75 (ITM#31412	b(	1680 1			H	140	560	5 250 300		2 35 40	28	25	2)		Н	+	0 33517	+		0 33516	-	No plugs required		) H	m ITM#		



# **ICC-ES Evaluation Report**

# **ESR-4931 LABC and LARC Supplement**

Reissued December 2022

Revised April 2023

This report is subject to renewal December 2023.

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A Subsidiary of the International Code Council®

DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

**DIVISION: 05 00 00—METALS** 

Section: 05 05 19—Post-Installed Concrete Anchors

**REPORT HOLDER:** 

**INVESTMENTS HARDWARE LIMITED (IHL)** 

# **EVALUATION SUBJECT:**

INVESTMENTS HARDWARE LIMITED (IHL) OCTOPLATINUM ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR SYSTEM IN CRACKED AND UNCRACKED CONCRETE

# 1.0 REPORT PURPOSE AND SCOPE

# Purpose:

The purpose of this evaluation report supplement is to indicate that the Investments Hardware Limited (IHL) OCTOPLATINUM Adhesive Anchor System and Post-Installed Reinforcing Bar System in cracked and uncracked concrete, described in ICC-ES evaluation report <a href="ESR-4931">ESR-4931</a>, have also been evaluated for compliance with the codes noted below as adopted by Los Angeles Department of Building and Safety (LADBS).

# Applicable code editions:

- 2020 City of Los Angeles Building Code (LABC)
- 2020 City of Los Angeles Residential Code (LARC)

# 2.0 CONCLUSIONS

The Investments Hardware Limited (IHL) OCTOPLATINUM Adhesive Anchor System and Post-Installed Reinforcing Bar System in cracked and uncracked concrete, described in Sections 2.0 through 7.0 of the evaluation report <a href="ESR-4931">ESR-4931</a>, comply with LABC Chapter 19, and LARC, and are subject to the conditions of use described in this report.

# 3.0 CONDITIONS OF USE

The Investments Hardware Limited (IHL) OCTOPLATINUM Adhesive Anchor System and Post-Installed Reinforcing Bar System described in this evaluation report must comply with all of the following conditions:

- All applicable sections in the evaluation report ESR-4931.
- The design, installation, conditions of use and labeling of the anchors are in accordance with the 2018 International Building
  Code® (IBC) provisions noted in the evaluation report ESR-4931.
- The design, installation and inspection are in accordance with additional requirements of LABC Chapters 16 and 17, as applicable.
- Under the LARC, an engineered design in accordance with LARC Section R301.1.3 must be submitted.
- The allowable and strength design values listed in the evaluation report and tables are for the connection of the anchors to
  the concrete. The connection between the anchors and the connected members shall be checked for capacity (which may
  govern).
- For use in wall anchorage assemblies to flexible diaphragm applications, anchors shall be designed per the requirements
  of City of Los Angeles Information Bulletin P/BC 2020-071.

This supplement expires concurrently with the evaluation report, reissued December 2022 and revised April 2023.





# **ICC-ES Evaluation Report**

# **ESR-4931 FBC Supplement**

Reissued December 2022 Revised April 2023 This report is subject to renewal December 2023.

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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

**DIVISION: 05 00 00—METALS** 

Section: 05 05 19—Post-Installed Concrete Anchors

**REPORT HOLDER:** 

**INVESTMENTS HARDWARE LIMITED (IHL)** 

### **EVALUATION SUBJECT:**

INVESTMENTS HARDWARE LIMITED (IHL) OCTOPLATINUM ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR SYSTEM IN CRACKED AND UNCRACKED CONCRETE

### 1.0 REPORT PURPOSE AND SCOPE

# Purpose:

The purpose of this evaluation report supplement is to indicate that the Investments Hardware Limited (IHL) OCTOPLATINUM adhesive anchors, described in ICC-ES evaluation report ESR-4931, have also been evaluated for compliance with the codes noted below.

# Applicable code editions:

- 2020 Florida Building Code—Building
- 2020 Florida Building Code—Residential

# 2.0 CONCLUSIONS

The IHL OCTOPLATINUM adhesive anchors, described in Sections 2.0 through 7.0 of the ICC-ES evaluation report ESR-4931, comply with the *Florida Building Code—Building* and the *Florida Building Code—Residential*. The design requirements are in accordance with the *Florida Building Code—Building* and the *Florida Building Code—Residential*, as applicable. The installation requirements noted in ICC-ES evaluation report ESR-4931 for the 2018 *International Building Code—Building and the Florida Building Code—Residential*, as applicable.

Use of the IHL OCTOPLATINUM adhesive anchors with stainless steel threaded rod materials and reinforcing bars has also been found to be in compliance with the High-Velocity Hurricane Zone provisions of the *Florida Building Code—Building* and the *Florida Building Code—Residential*, with the following condition:

 For anchorage to wood members, the connection subject to uplift must be designed for no less than 700 pounds (3114 N).

Use of the IHL OCTOPLATINUM adhesive anchors with carbon steel standard steel threaded rod materials for compliance with the High-velocity Hurricane Zone provisions of the *Florida Building Code—Building* and the *Florida Building Code—Residential* has not been evaluated and is outside the scope of the supplemental report, with the following condition:

 a) For anchorage to wood members, the connection subject to uplift must be designed for no less than 700 pounds (3114 N).

For products falling under Florida Rule 61G20-3, verification that the report holder's quality assurance program is audited by a quality assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official, when the report holder does not possess an approval by the Commission).

This supplement expires concurrently with the evaluation report, reissued December 2022 and revised April 2023.

